

ENERGETSKI STROJI

Uvod

Pregled teoretičnih osnov

Hidrostatika

Dinamika tekočin

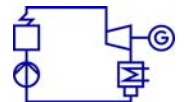
Termodinamika

Podobnostni zakoni

Volumetrični stroji

Turbinski stroji

Energetske naprave



TERMODINAMIKA

Zakon o ohranitvi energije

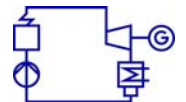
Krožni procesi

Delo, moč in izkoristek

Tok tekočine skozi šobe

Prenos toplote

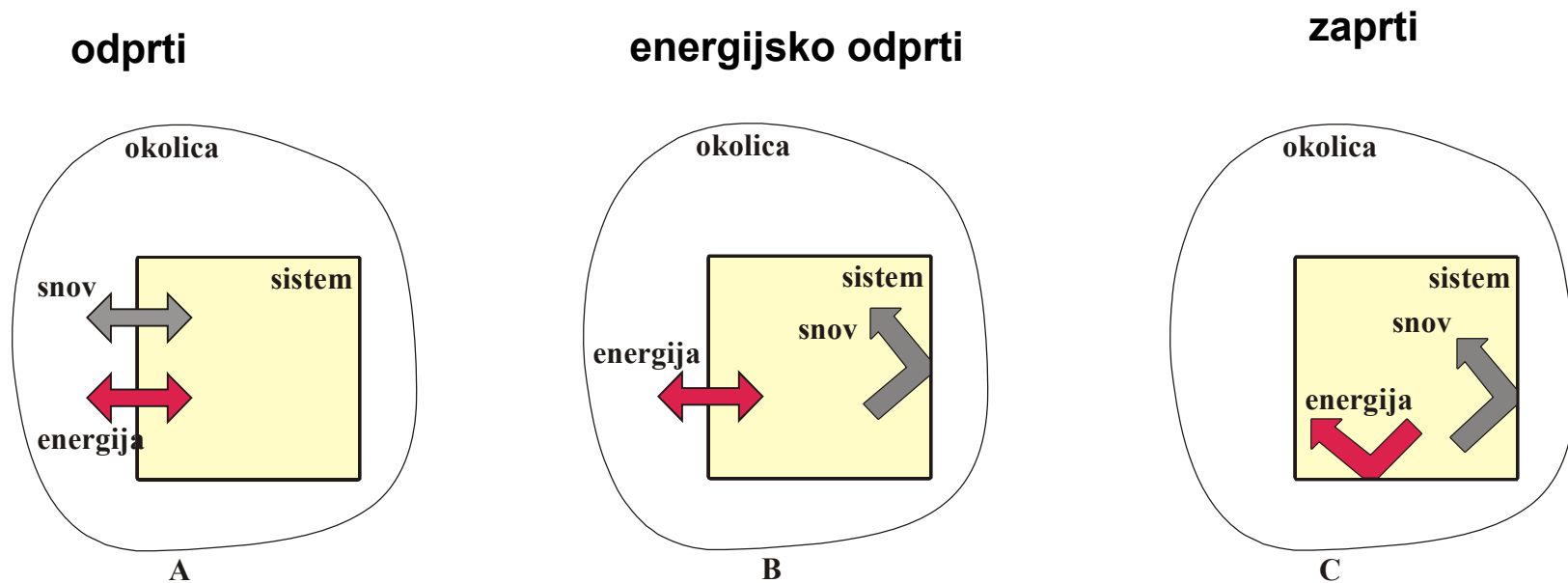
Goriva in zgorevanje



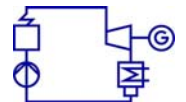
Zakon o ohranitvi energije

termodinamski sistemi

- Izoliran sistem: vsota energij (eksergij, anergij) je konstantna
- Sistem je omejen s stenami (prehod mase in energij)
- Sistem je obdan z okolico, s katero izmenjuje maso in energijo
- Delo W in toplote Q delujeta na *meji* sistema

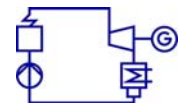
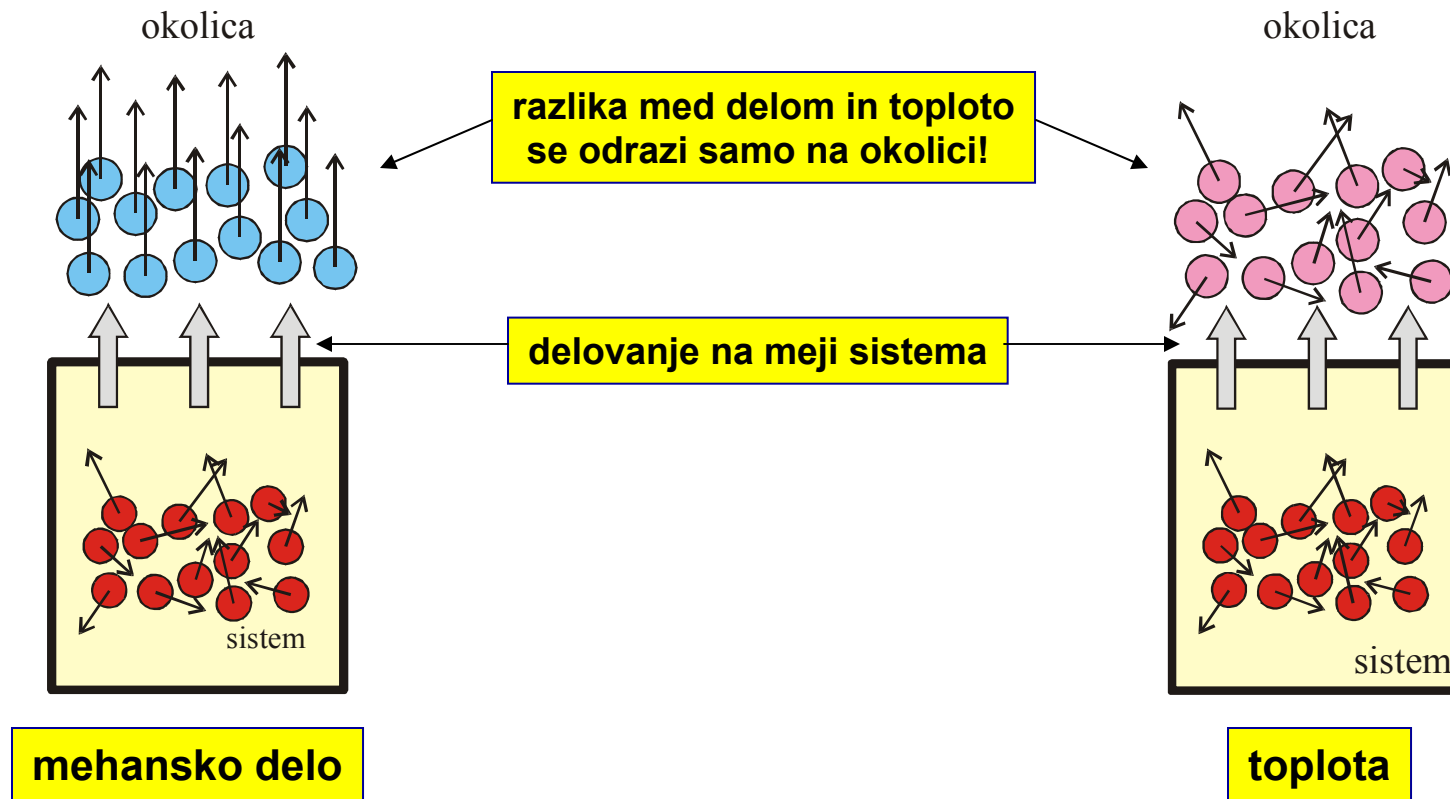


energija, ki prehaja *mejo* sistema – prehodna energija: *mehansko delo* in *toplota*



Zakon o ohranitvi energije

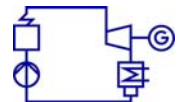
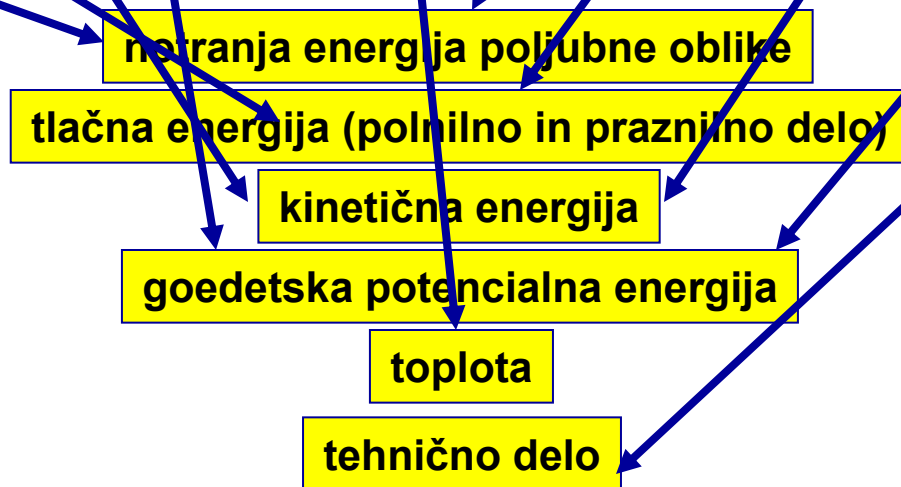
sistem in okolica – mehansko delo in toplota



Zakon o ohranitvi energije

energijska bilanca splošne preobrazbe sistema

$$U_1 + p_1 \cdot V_1 + m \cdot \frac{v_1^2}{2} + m \cdot g \cdot H_1 + Q_{12} = U_2 + p_2 \cdot V_2 + m \cdot \frac{v_2^2}{2} + m \cdot g \cdot H_2 + W_{t12}$$



Zakon o ohranitvi energije

posebni primeri

Bernoullijeva enačba:

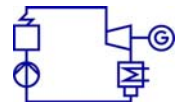
$$U_1 + p_1 \cdot V_1 + m \cdot \frac{v_1^2}{2} + m \cdot g \cdot H_1 + Q_{12} = U_2 + p_2 \cdot V_2 + m \cdot \frac{v_2^2}{2} + m \cdot g \cdot H_2 + W_{t12}$$

nestisljiva tekočina brez trenja

adiabatni tok: brez dovoda in odvoda toplote

brez pridobljenega ali porabljenega (tehničnega) dela

$$p_1 \cdot V_1 + m \cdot \frac{v_1^2}{2} + m \cdot g \cdot H_1 = p_2 \cdot V_2 + m \cdot \frac{v_2^2}{2} + m \cdot g \cdot H_2$$



Zakon o ohranitvi energije

posebni primeri

opravljanje tehničnega dela iz notranje energije
(stacionarna preobrazba iz mirujočega stanja):

$$U_1 + p_1 \cdot V_1 + m \cdot \frac{v_1^2}{2} + m \cdot g \cdot H_1 + Q_{12} = U_2 + p_2 \cdot V_2 + m \cdot \frac{v_2^2}{2} + m \cdot g \cdot H_2 + W_{t12}$$

$$Q_{12} - W_{t12} = (U_2 + p_2 \cdot V_2) - (U_1 + p_1 \cdot V_1)$$

ENTALPIJA SNOVI
V KONČNEM STANJU

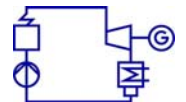
ENTALPIJA SNOVI
V ZAČETNEM STANJU

$$Q_{12} - W_{t12} = m \cdot (h_2 - h_1)$$

Entalpija je veličina stanja!

Energijo odprtega sistema:

- poveča dovedena toplota
- zmanjša iz sistema pridobljeno delo



Zakon o ohranitvi energije

posebni primeri

delo enkratne ekspanzije (absolutno delo)

$$U_1 + p_1 \cdot V_1 + m \cdot \frac{v_1^2}{2} + m \cdot g \cdot H_1 + Q_{12} = U_2 + p_2 \cdot V_2 + m \cdot \frac{v_2^2}{2} + m \cdot g \cdot H_2 + W_{t12}$$

polnilno delo

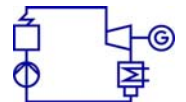
praznilno delo

Absolutno delo

$$W_{u12} = W_{t12} - p_1 \cdot V_1 + p_2 \cdot V_2$$

Tehnično delo, zaprt sistem:

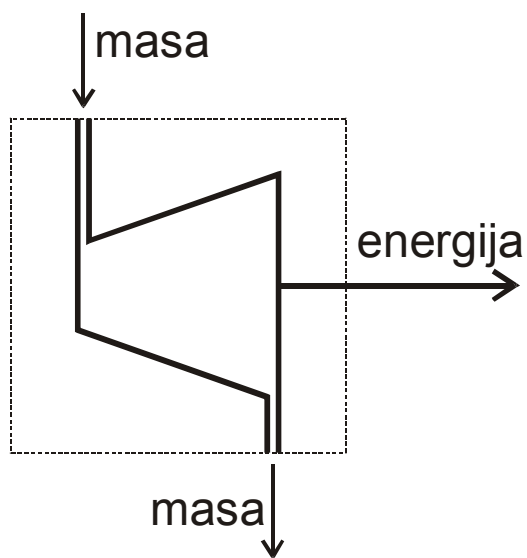
$$W_{t12} = 0 \Rightarrow Q_{12} - W_{t12} = U_2 - U_1$$



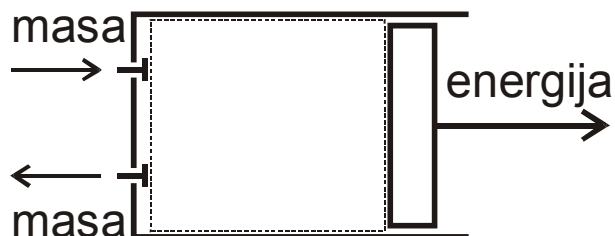
Zakon o ohranitvi energije

polnilno in praznilno delo

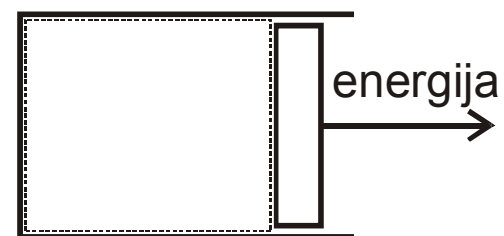
A turbinski stroj



B volumenski stroj



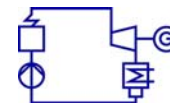
C volumenski stroj



neprekinjeno polnjenje
in praznjenje

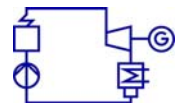
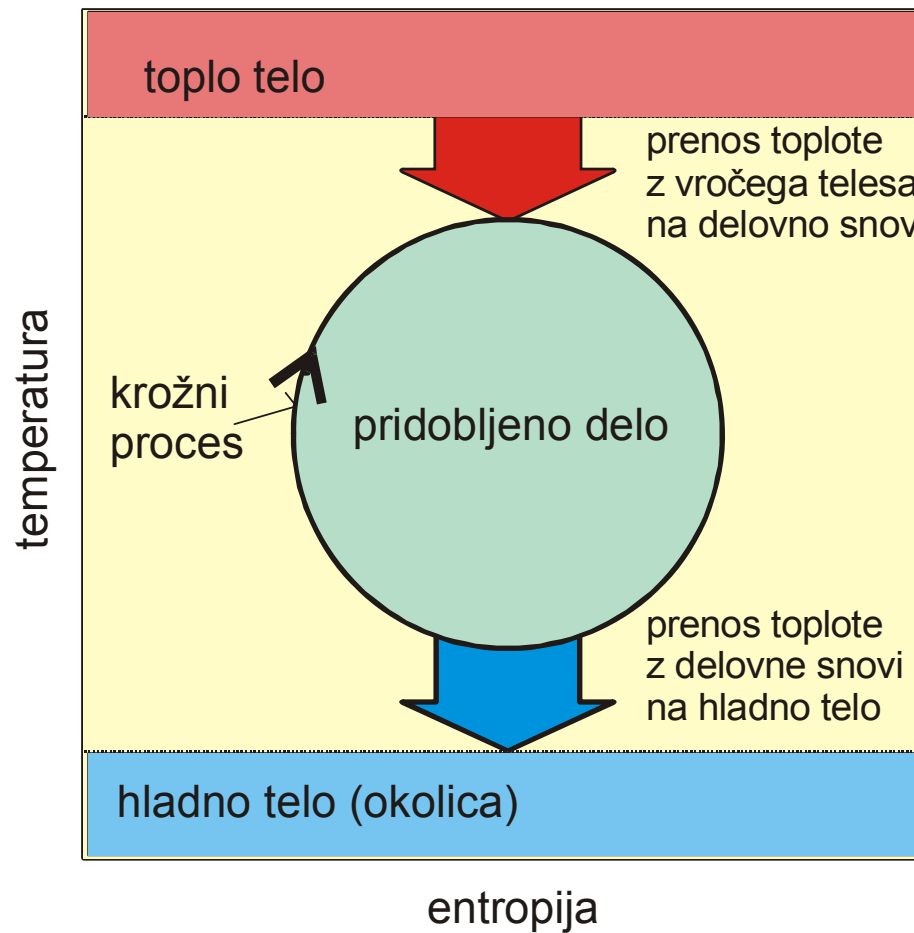
periodično polnjenje
in praznjenje

brez polnjenja
in praznjenja



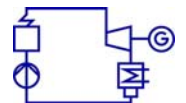
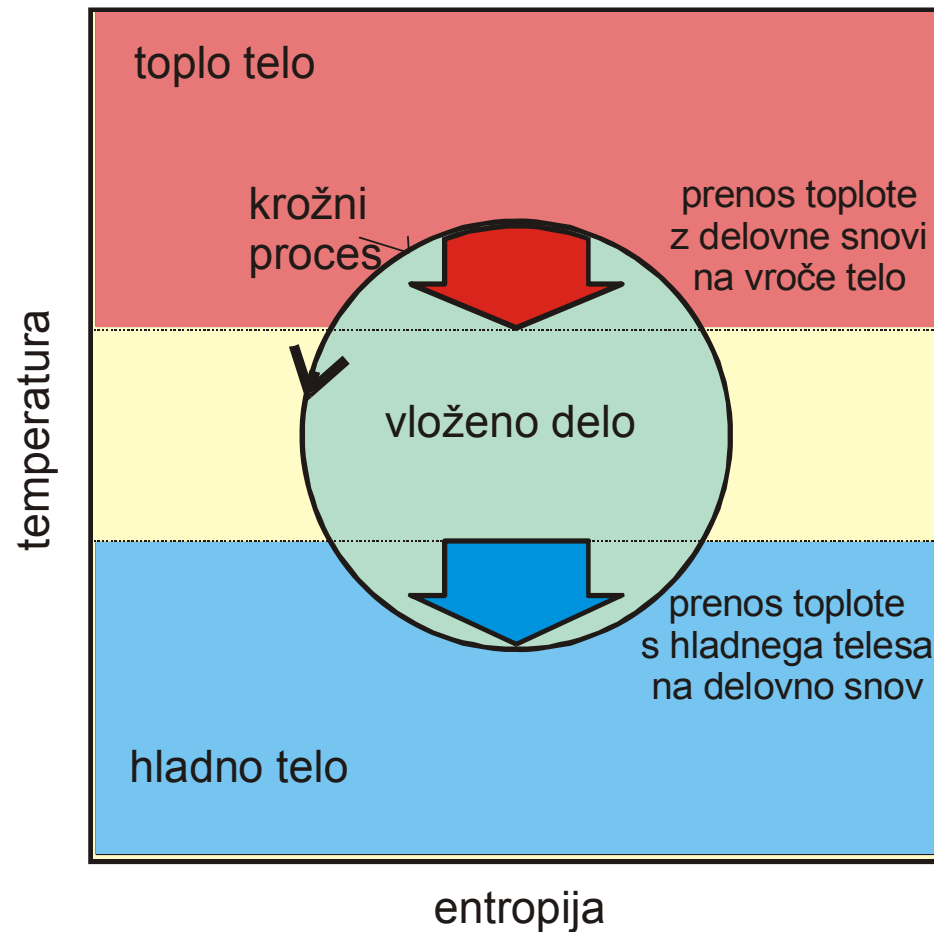
Krožni procesi

desni krožni procesi – toplotni stroji



Krožni procesi

levi krožni procesi – hladilni stroji



Krožni procesi

primerjalni krožni procesi

Pogoste predpostavke:

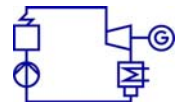
- idealni plin
- povračljive preobrazbe

Periodično delujoči stroji (volumenski toplotni stroji)

- vse preobrazbe se izvedejo v enem samem stroju
- uporaba diagrama $p - v$

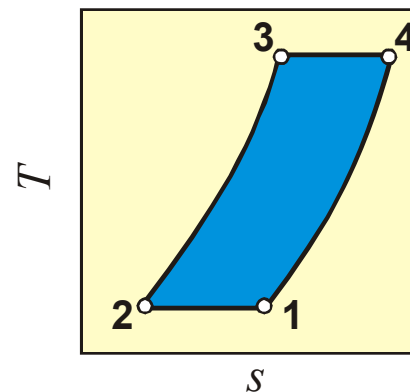
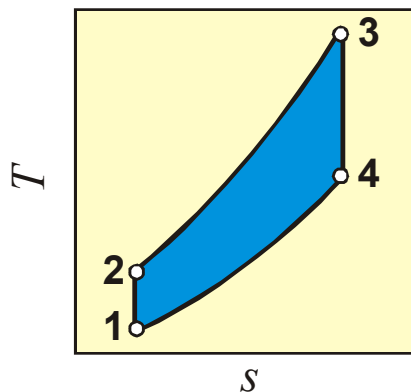
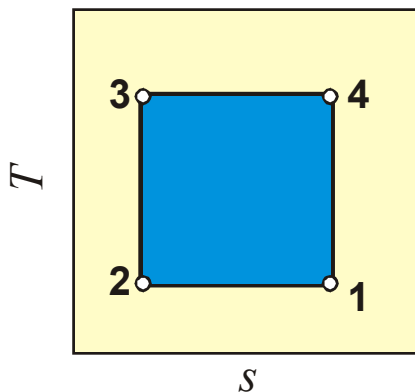
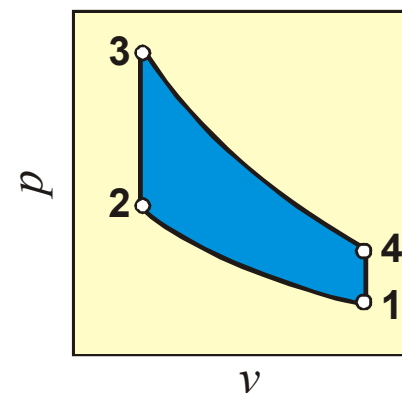
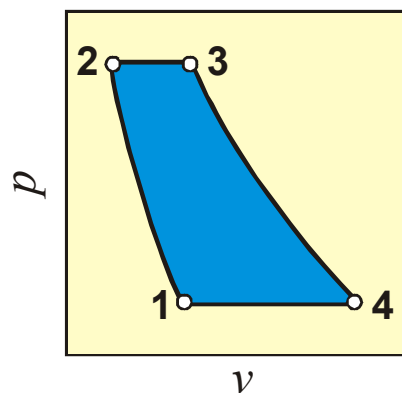
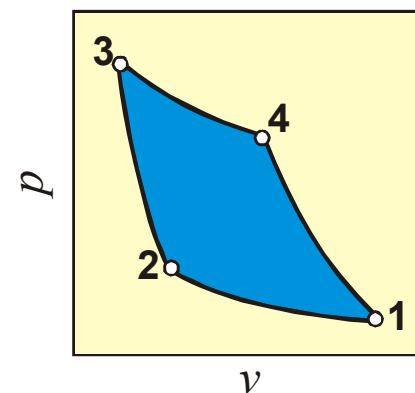
Zvezno delujoči (turbinski) stroji (toplotno postrojenje)

- posamezne preobrazbe se izvedejo v ločenem stroju
- povezovanje strojev v postroje in postrojenja
- uporaba diagramov: $T - s$ (idealni plin)
 $h - s$ (realni plin)



Krožni procesi

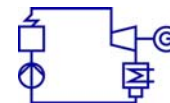
primerjalni krožni procesi



Carnot

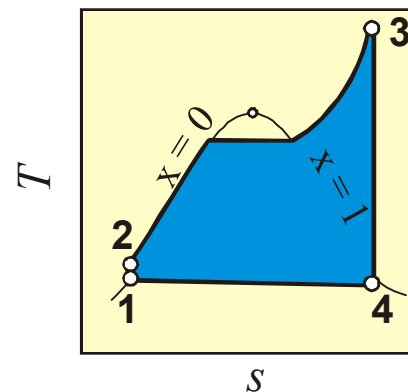
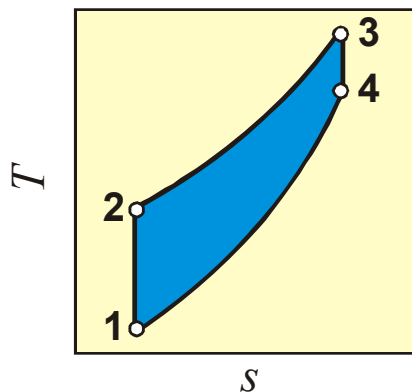
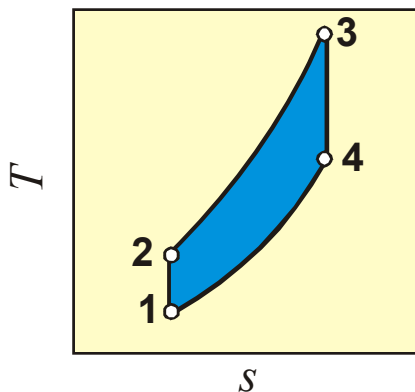
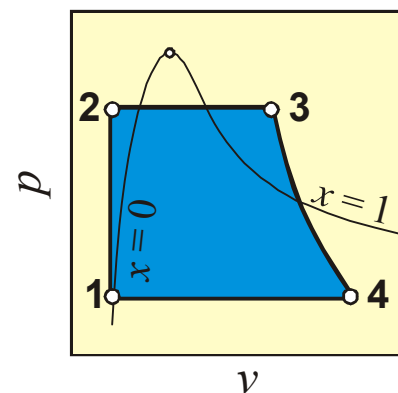
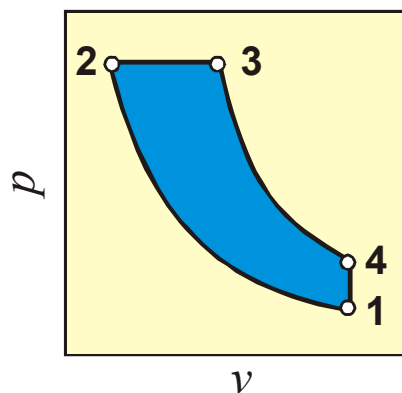
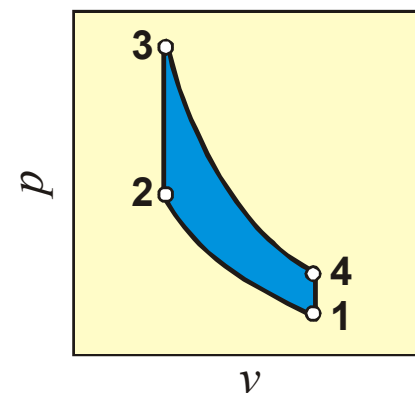
Joule

Stirling



Krožni procesi

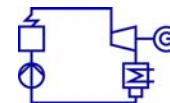
primerjalni krožni procesi



Otto

Diesel

Clausius – Rankine



Mollierov h - s diagram

prednosti za tehniško uporabo

1. glavni stavek termodinamike

$$dq = T \cdot ds = dh - v \cdot dp$$

izobarni dovod toplote

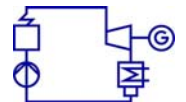
$$dp = 0 \Rightarrow Tds = dh = dq$$

Pri konstantnem tlaku dovedena (odvedena) toplota je enaka razliki entalpij snovi, ki ji doploto dovajamo (odvajamo).

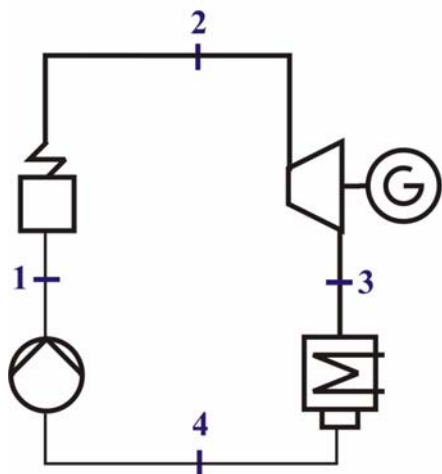
adiabatna delovan preobrazba (kompresija, ekspanzija)

$$dq = 0 \Rightarrow vdp = dh$$

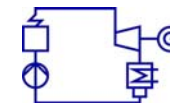
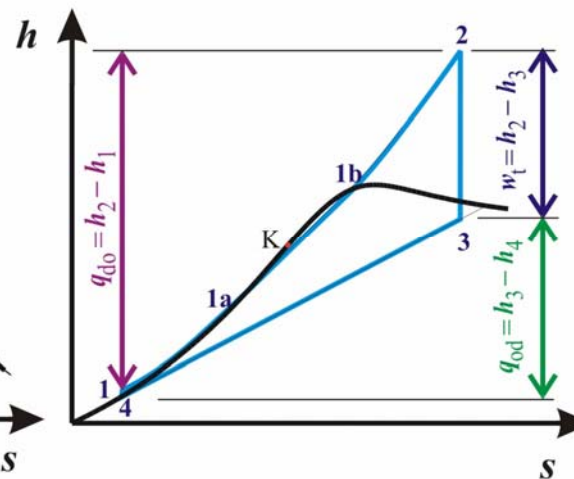
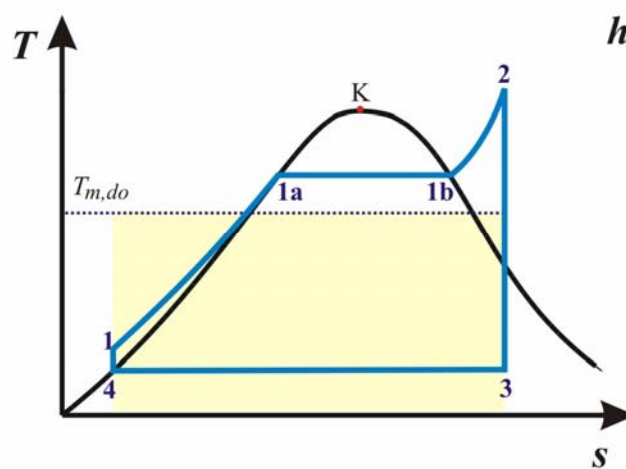
Ob adiabatni pridobljeno ali porabljeno tehnično delo je enako entalpijski razliki snovi, ki je podvržena preobrazbi.



Primer: parni krožni proces



- 1 → 1a izobarno segrevanje vode
- 1a → 1b uparjanje vode: $p = \text{konst}$; $T = \text{konst}$
- 1b → 2 izobarno pregrevanje pare
- 2 → 3 izentropna ekspanzija
- 3 → 4 odvod toplote (kondenzacija): $p = \text{konst}$; $T = \text{konst}$
- 4 → 1 dvig tlaka v črpalcki

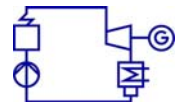
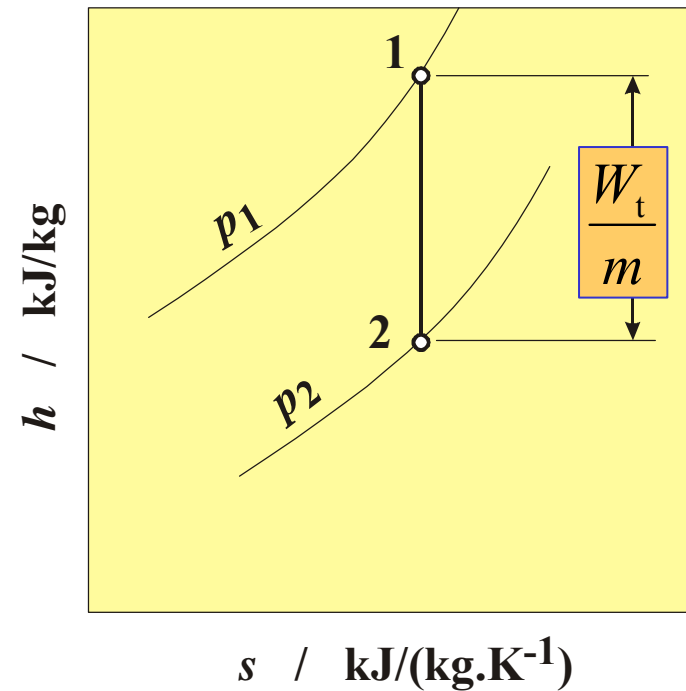
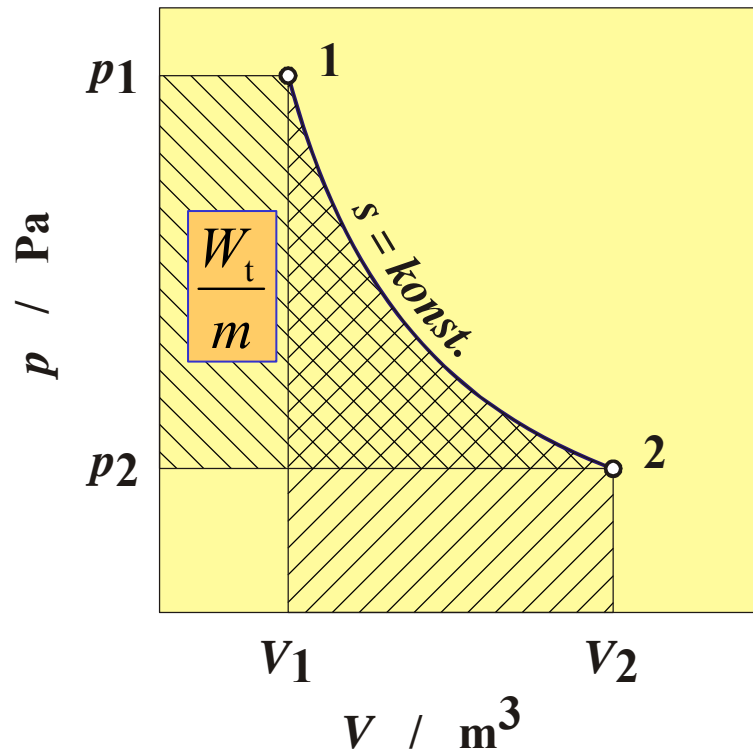


Krožni procesi

delo

Tehnično delo preobrazbe:

$$W_t = \int_{p_1}^{p_2} v \cdot dp$$



Krožni procesi

delo, moč

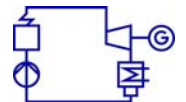
Delo krožnega procesa:

V krožnem procesu pridobljeno tehnično delo (ekspanzije),
zmanjšano za porabljeno tehnično delo (kompresije)

$$W = W_{tE} - W_{tK}$$

Moč krožnega procesa:

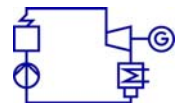
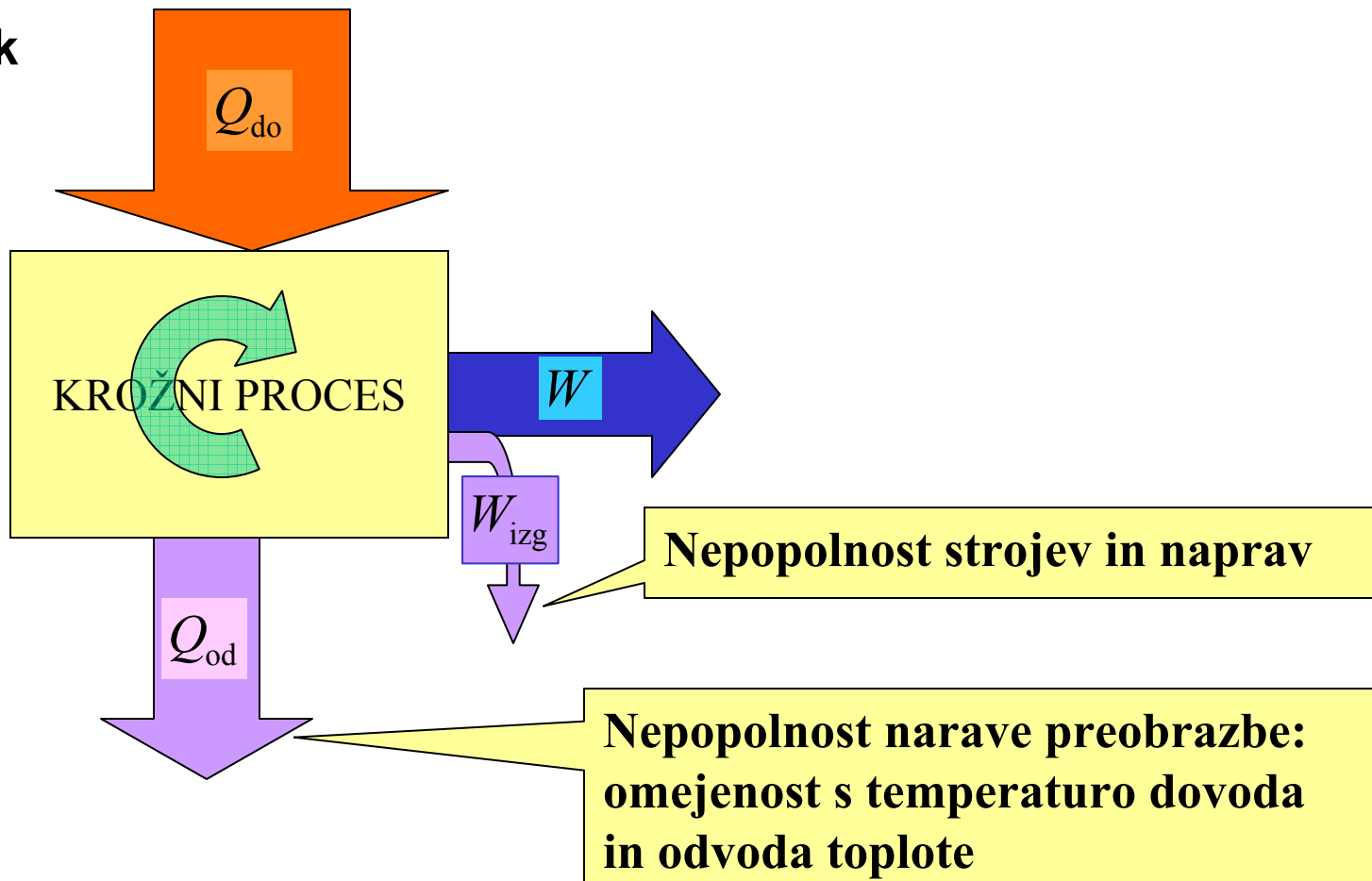
$$P = \frac{dW}{dt} = \dot{W}$$



Krožni procesi

Učinkovitost pretvorbe energije v krožnem procesu

izkoristek

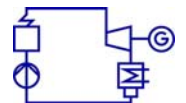


Izkoristek: merilo za učinkovitost preobrazbe

$$\text{IZKORISTEK} = \frac{\text{IZKORIŠČENA ENERGIJA (MOČ)}}{\text{VLOŽENA ENERGIJA (MOČ)}}$$

POGONSKI STROJ: PRIDOBLJENO DELO JE MANJŠE OD TEORETIČNEGA

DELOVNI STROJ: PORABLJENO DELO JE VEČJE OD TEORETIČNEGA



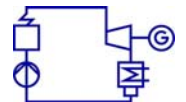
TOPLOTNI KROŽNI PROCESI – PRETVORBA TOPLOTE V MEHANSKO DELO

Termični izkoristek krožnega procesa

$$\eta_c = \frac{P_{th}}{Q_{Go}} = \frac{P_{th}}{m_{Go} \cdot H_i}$$

P_{th} ... prosta moč krožnega procesa pri povračljivih preobrazbah

- **upošteva neopolnost narave preobrazbe**
- **pretežni del nepovračljivosti enostavnih krožnih procesov**



Notranji (indicirani) izkoristek

pogonski stroj:

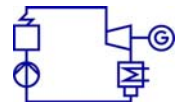
$$\eta_i = \frac{P_i}{P_{th}}$$

delovni stroj:

$$\eta_i = \frac{P_{th}}{P_i}$$

P_i ... prosta moč krožnega procesa pri dejanskih (politropnih) preobrazbah ali teoretična moč (na gredi) stroja

- upošteva neopolnost kompresij in ekspanzij v strojih (nepopolnost prenosa mehanske energije s fluida na gred)
- stiskanje kapljev in ekspanzija plinov (par ugodna)



Mehanski izkoristek

pogonski stroj:

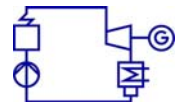
$$\eta_m = \frac{P_m}{P_i}$$

delovni stroj:

$$\eta_m = \frac{P_i}{P_m}$$

P_m ... dejanska prosta moč krožnega procesa
ali dejanska moč na gredi stroja

- upošteva neopolnost prenosa mehanske moči gredi
(ležaji, tesnila,...)



Dejanski (efektivni izkoristek)

pogonski stroj:

$$\eta_e = \frac{P_m}{Q_{do}} = \prod_j \eta_j$$

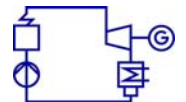
delovni stroj:

$$\eta_e = \frac{P_{th}}{P_m} = \prod_i \eta_i$$

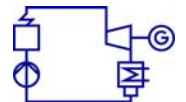
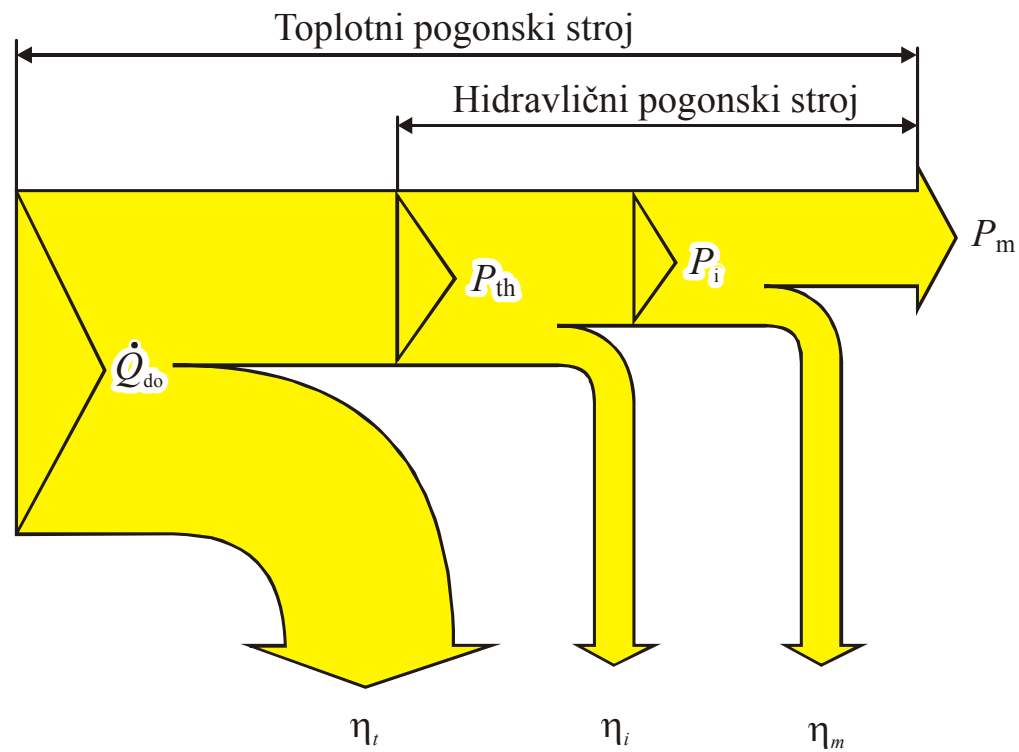
produkt izkoristkov vseh pretvorb – od začetnega do končnega stanja

- upošteva uspešnost narave pretvorbe in
- pretvorb v posameznih strojih in napravah

- različne definicije za vsak posamičen primer



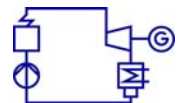
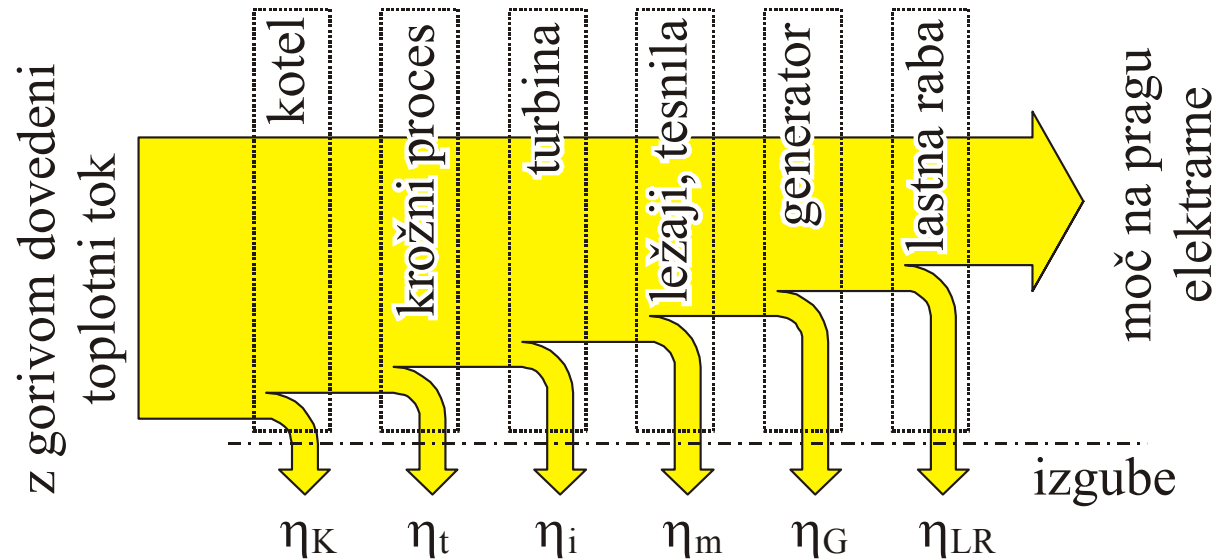
Izkoristek celotne pretvorbe



Primeri: PRETVORBA ENERGIJE V TERMOELEKTRARNI

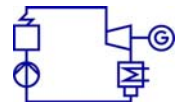
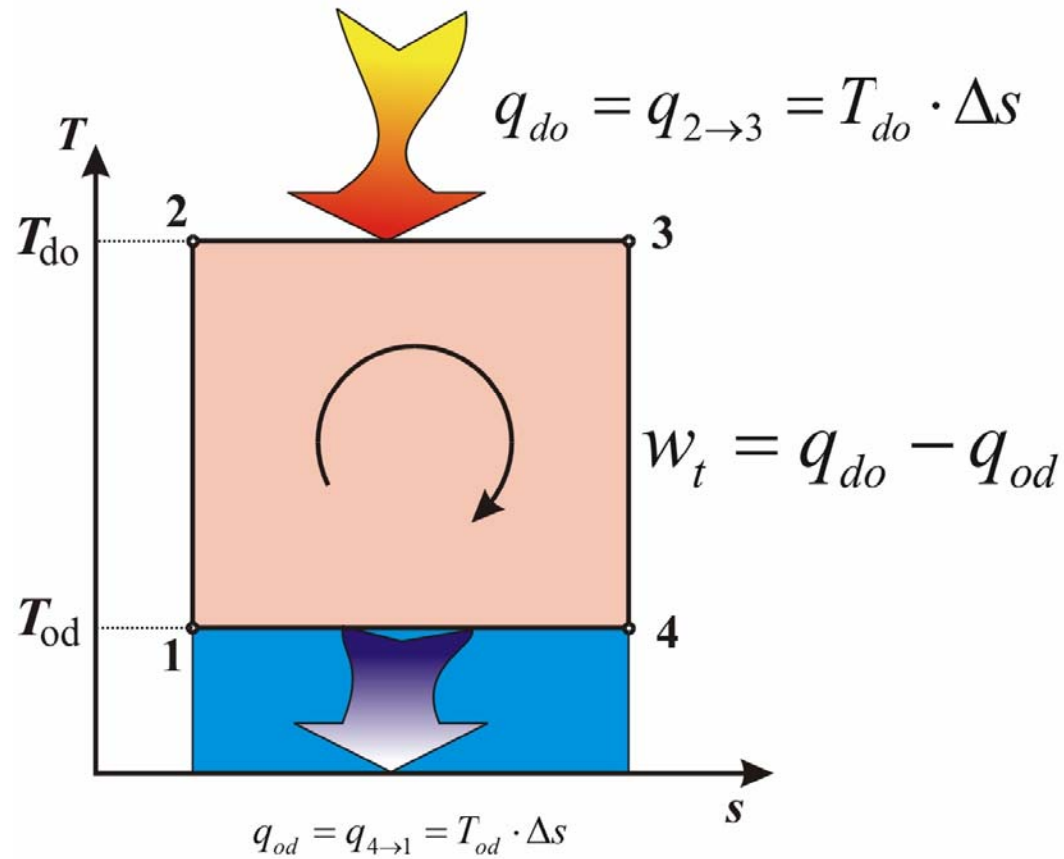
$$\eta_e = \underbrace{\frac{\dot{Q}_G}{\dot{Q}_K}} \cdot \underbrace{\frac{\dot{Q}_K}{W_{Tid}}} \cdot \underbrace{\frac{P_{Tid}}{P_T}} \cdot \underbrace{\frac{P_T}{P_m}} \cdot \underbrace{\frac{P_m}{P_G}} \cdot \underbrace{\frac{P_G}{P_E}}$$

$$\eta_e = \eta_K \cdot \eta_t \cdot \eta_i \cdot \eta_m \cdot \eta_G \cdot \eta_{LR}$$

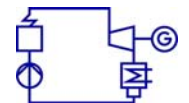
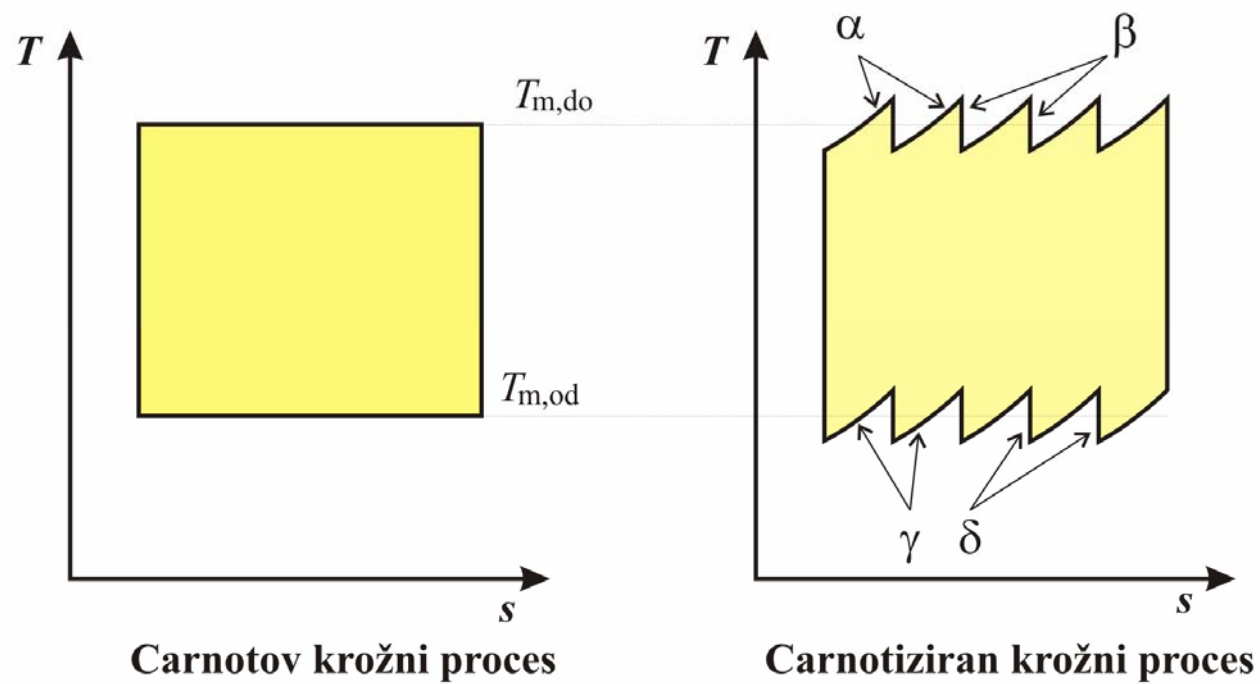


Princip optimiranja krožnih procesov

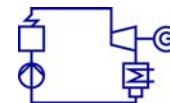
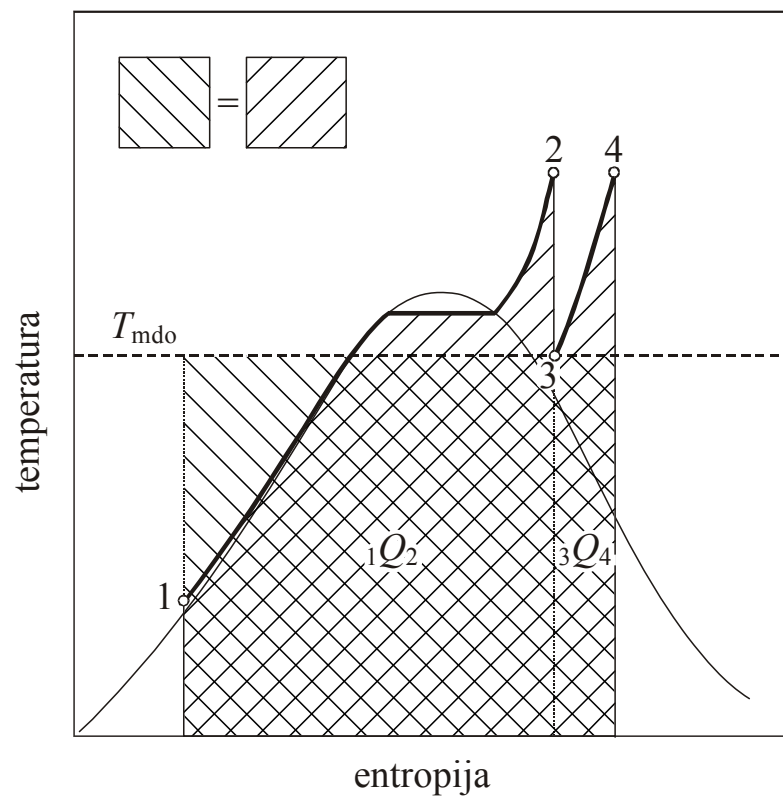
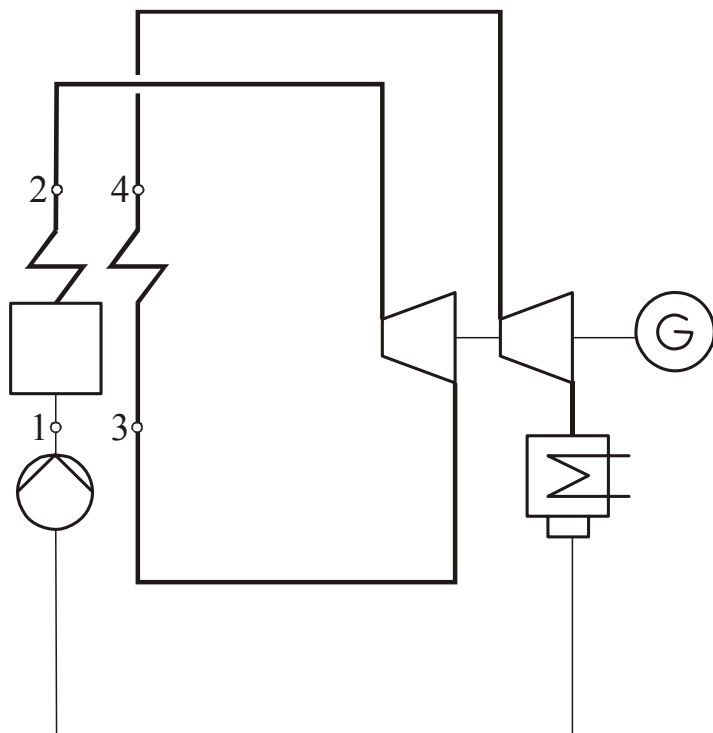
Carnotov krožni proces



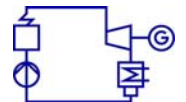
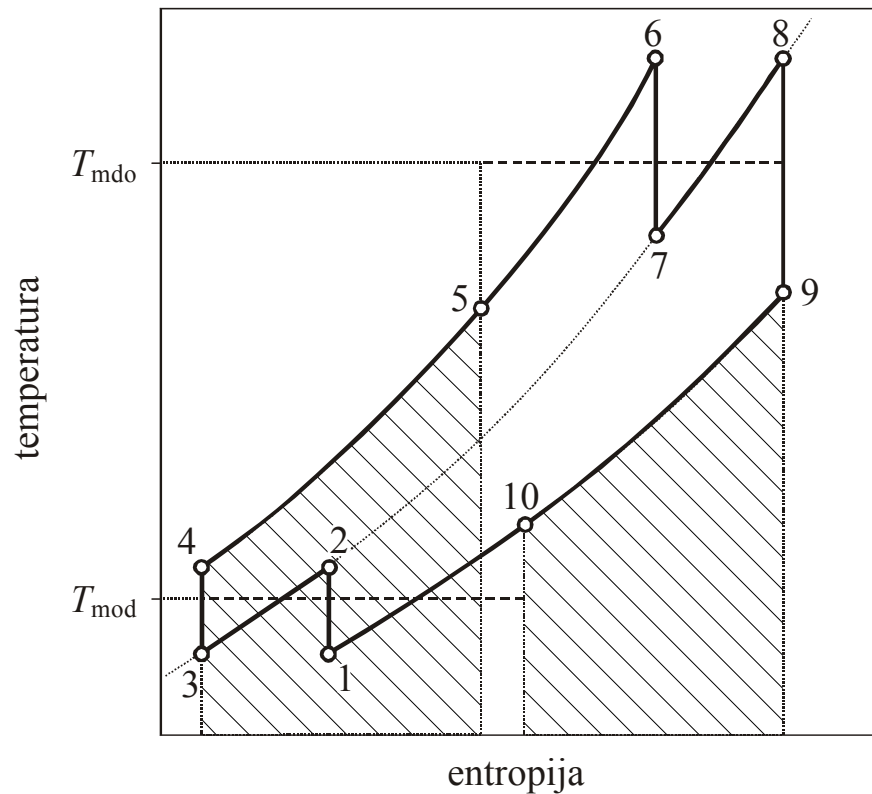
Carnotiziranje (optimiranje) poljubnega krožnega procesa



Primer: ponovno pregrevanje pare



Primer: Joulov plinski proces – vmesno hlajenje kompresije, sekvenčno zgorevanje (dovod toplote), regeneracija toplote



Tok tekočine skozi šobe

Tok plina skozi kanal: energijska enačba

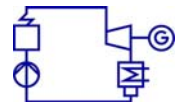
$$U_1 + p_1 \cdot V_1 + m \cdot \frac{v_1^2}{2} + m \cdot g \cdot H_1 + Q_{12} =$$
$$U_2 + p_2 \cdot V_2 + m \cdot \frac{v_2^2}{2} + m \cdot g \cdot H_2 + W_{t12}$$

Izentropni tok brez opravljanja dela:

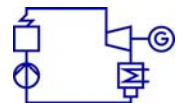
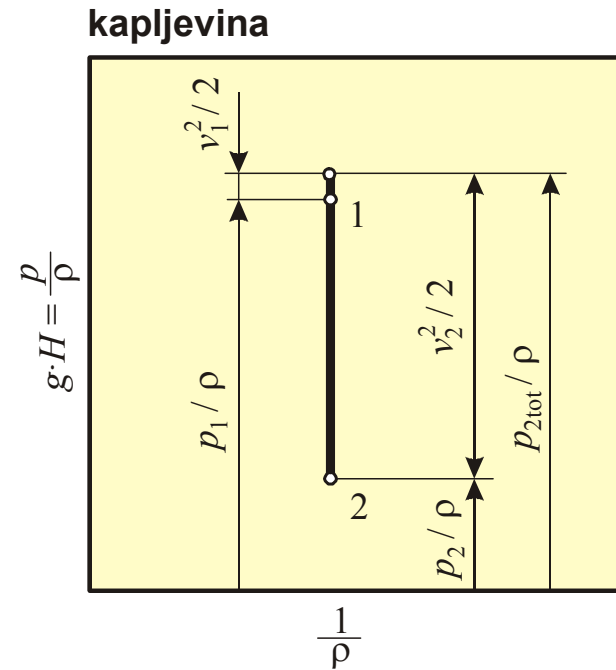
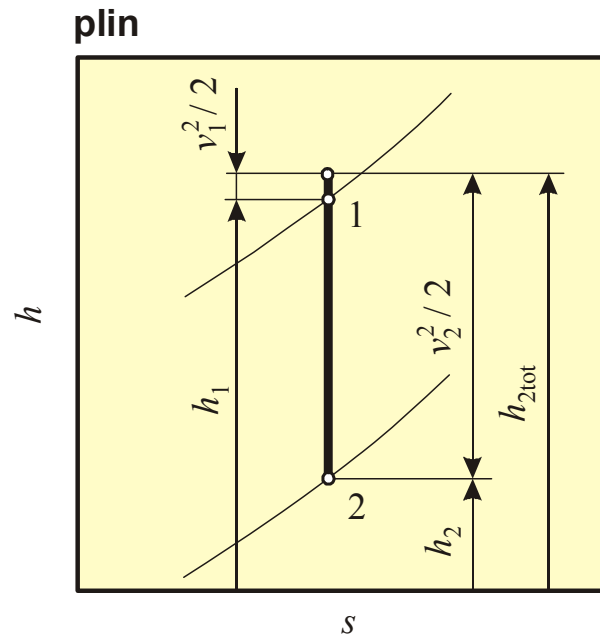
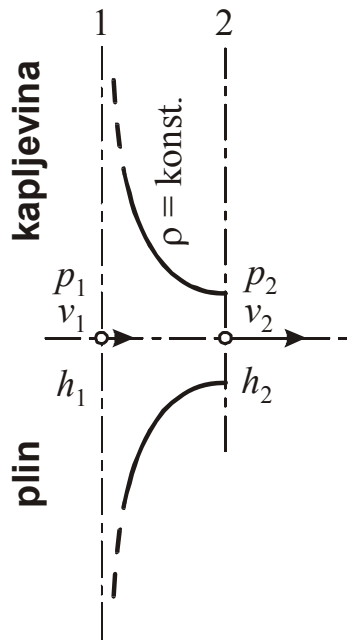
$$U_1 + p_1 \cdot V_1 + m \cdot \frac{v_1^2}{2} = U_2 + p_2 \cdot V_2 + m \cdot \frac{v_2^2}{2}$$

Totalna entalpija se ohranja:

$$h_1 + \frac{v_1^2}{2} = h_2 + \frac{v_2^2}{2}$$



Tok tekočine skozi šobe



HITROST IZTEKANJA PLINA

**Pospeševanje toka skozi konfuzor
(primer šoba v vodilniku parne turbinske stopnje)**

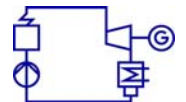
$$v_2 = \sqrt{v_1^2 + 2 \cdot (h_1 - h_2)}$$

poenostavitev:

$$v_1^2 \ll v_2^2 \Rightarrow v_2 = \sqrt{2 \cdot (h_1 - h_2)}$$

**za nestisljive tekočine:
(primer šoba Peltonove turbine)**

$$\rho_1 = \rho_2 = \rho \Rightarrow v_2 = \sqrt{2 \cdot \frac{p_1 - p_2}{\rho}}$$



Iztekanje idealnega plina

$$v_2 = \sqrt{2 \cdot (h_1 - h_2)} = \sqrt{2 \cdot c_p \cdot (T_1 - T_2)}$$

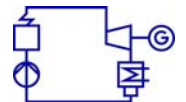
$$c_p = \left. \frac{\delta h}{\delta T} \right|_{p=\text{konst.}}$$

enačba stanja idealnega plina:

$$T = \frac{p}{\rho \cdot R}$$

izentropna ekspanzija:

$$\frac{T_2}{T_1} = \left(\frac{p_2}{p_1} \right)^{\frac{\kappa-1}{\kappa}}$$



Iztekanje idealnega plina

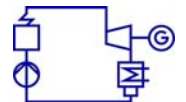
$$v_2 = \sqrt{2 \cdot \frac{\kappa}{\kappa - 1} \cdot \frac{p_1}{\rho_1} \cdot \left[1 - \left(\frac{p_2}{p_1} \right)^{\frac{\kappa - 1}{\kappa}} \right]}$$

kontinuitetna enačba:

$$\dot{m} = \rho_2 \cdot v_2 \cdot A$$

gostota masnega toka skozi šobo:

$$\frac{\dot{m}}{A} = \sqrt{2 \cdot \rho_1 \cdot p_1} \cdot \sqrt{\frac{\kappa}{\kappa - 1} \cdot \left[\left(\frac{p}{p_1} \right)^{\frac{2}{\kappa}} - \left(\frac{p}{p_1} \right)^{\frac{\kappa + 1}{\kappa}} \right]} = \sqrt{2 \cdot \rho_1 \cdot p_1} \cdot \Psi$$

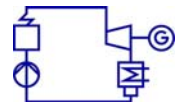


Pretočna funkcija

$$\Psi = \sqrt{\frac{\kappa}{\kappa - 1}} \cdot \left[\left(\frac{p_2}{p_1} \right)^{\frac{2}{\kappa}} - \left(\frac{p_2}{p_1} \right)^{\frac{\kappa+1}{\kappa}} \right]$$

Nižle pretočne funkcije: $\Psi = 0; \frac{p_2}{p_1} = 0$ $p_2 = 0$

$\Psi = 0; \frac{p_2}{p_1} = 1$ $p_2 = p_1$



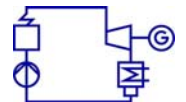
Maksimum pretočne funkcije:

$$\frac{\partial \Psi}{\partial \left(\frac{p_2}{p_1} \right)} = 0$$

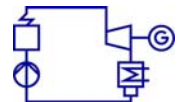
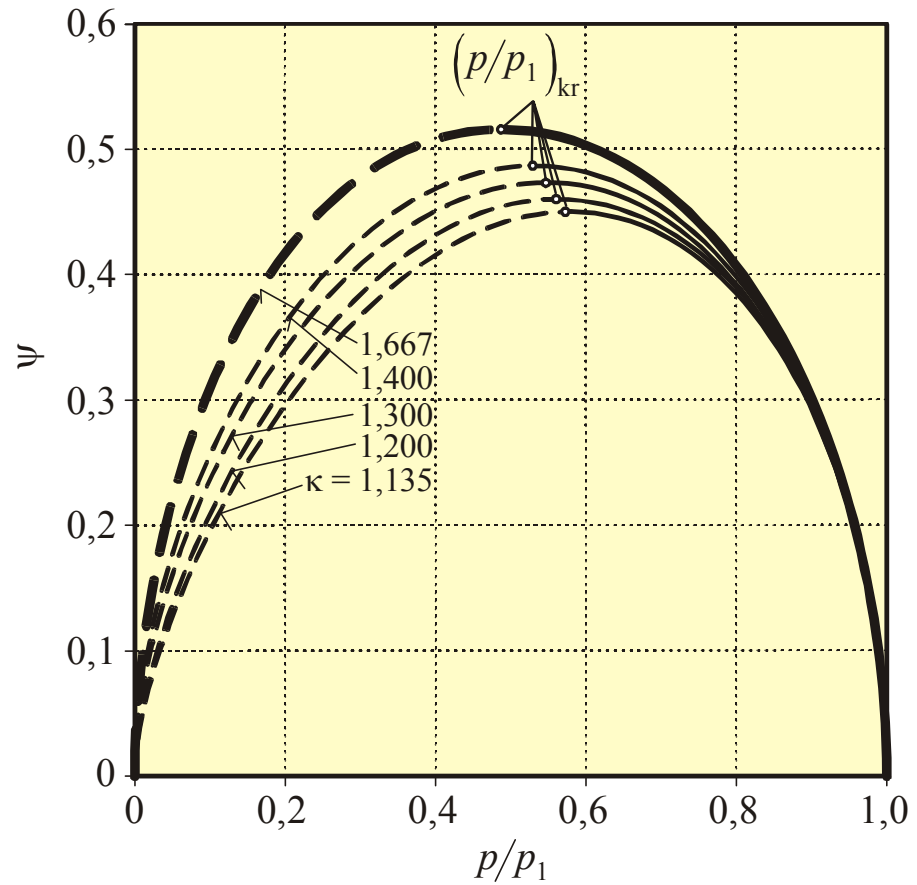
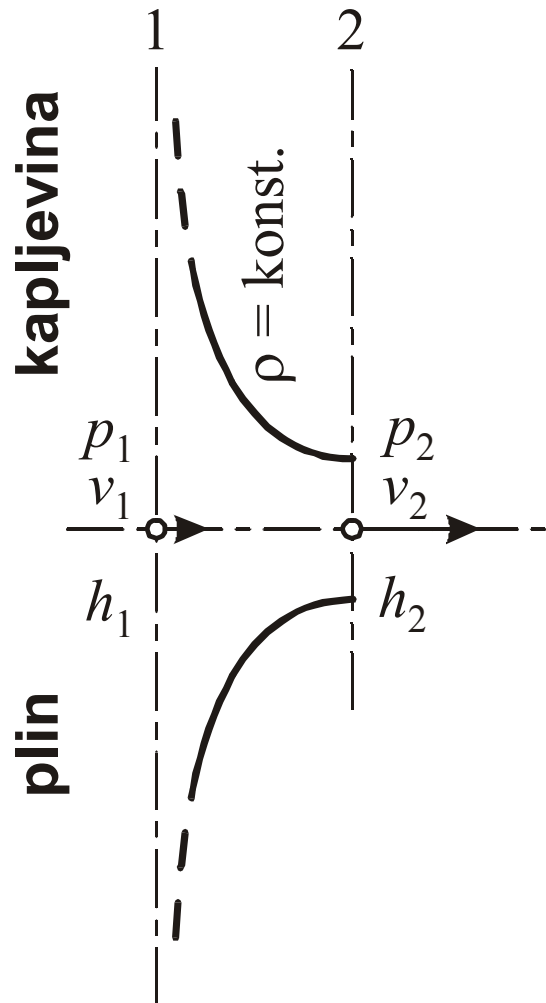
$$\Psi_{\max} = \left(\frac{2}{\kappa + 1} \right)^{\frac{\kappa}{\kappa - 1}} \sqrt{\frac{\kappa}{\kappa + 1}}$$

Kritično (Lavalovo) tlačno razmerje:

$$\left(\frac{p_2}{p_1} \right)_{\text{kr}} = \left(\frac{2}{\kappa + 1} \right)^{\frac{\kappa}{\kappa - 1}}$$

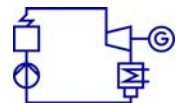


Iztekanje idealnega plina



Iztekanje idealnega plina

Vrsta plina	κ	$(p_1/p_2)_{kr}$	Ψ_{max}
enoatomni plin	1,667	0,487	0,514
dvoatomni plin (zrak)	1,400	0,528	0,484
triatomni plin (pregreta para)	1,300	0,546	0,472



Kontinuitetna enačba

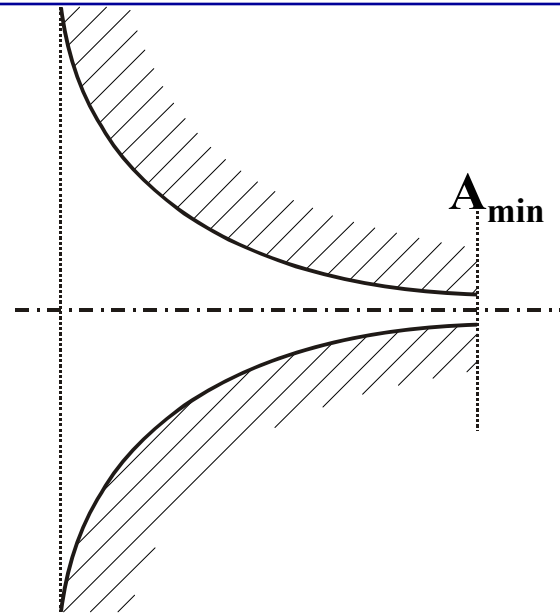
$$\dot{m} = A \cdot \Psi \cdot \sqrt{2 \cdot \rho_1 \cdot p_1} = \text{konst.}$$

Konvergentna šoba:

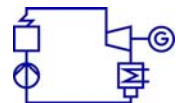
$$\frac{dA}{dl} < 0$$

$$\left(\frac{p_2}{p_1} \right) > \left(\frac{p_2}{p_1} \right)_{\text{kr}}$$

$$\left(\frac{p_2}{p_1} \right) < \left(\frac{p_2}{p_1} \right)_{\text{kr}} \Rightarrow \Psi < \Psi_{\text{max}} \Rightarrow \frac{dA}{dl} > 0$$



Na najožjem preseku konvergentne šobe ne more vladati manjši tlak kot je kritični (Lavalov)



Kritično (Lavalovo) tlačno razmerje

$$\left(\frac{p_2}{p_1}\right) = \left(\frac{p_2}{p_1}\right)_{\text{kr}}$$

Zvočna hitrost

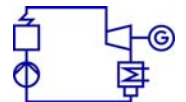
$$v_{\text{kr}} = \sqrt{\kappa \cdot R \cdot T_2}$$

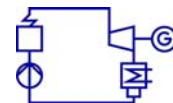
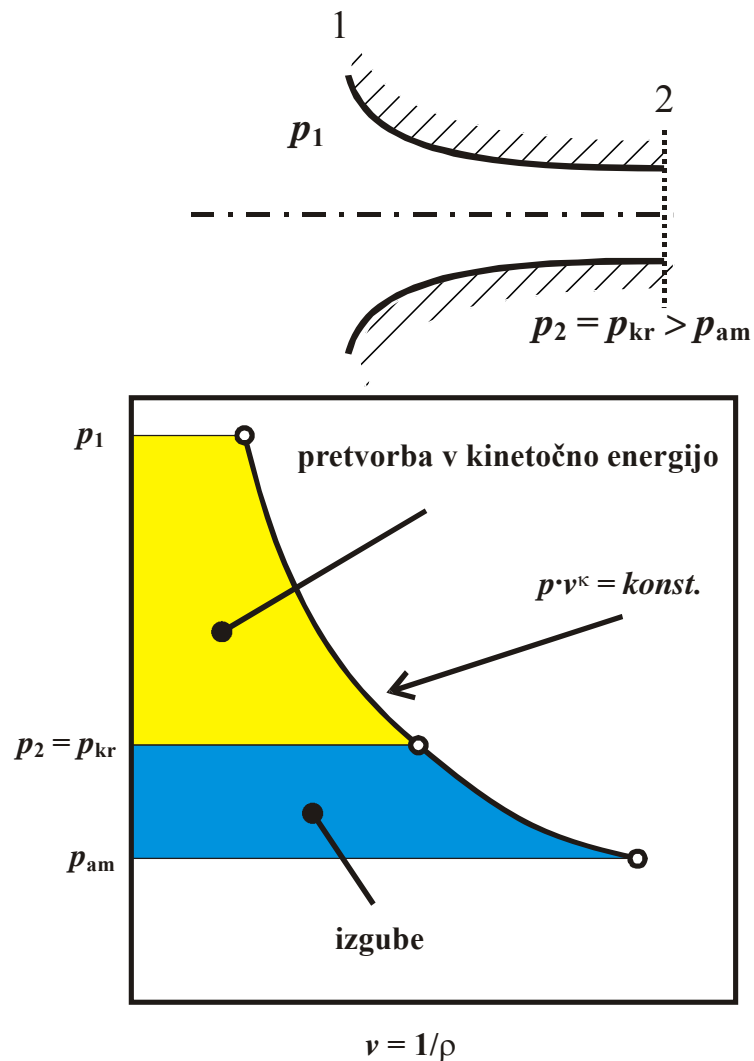
Na najožjem preseku konvergentne šobe hitrost ne more biti večja od zvočne (Lavalove) hitrosti

Machovo število

$$\text{Ma} = \frac{v}{v_{\text{kr}}} = \frac{\text{lokalna hitrost}}{\text{lokalna zvočna hitrost}}$$

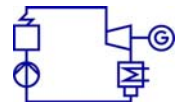
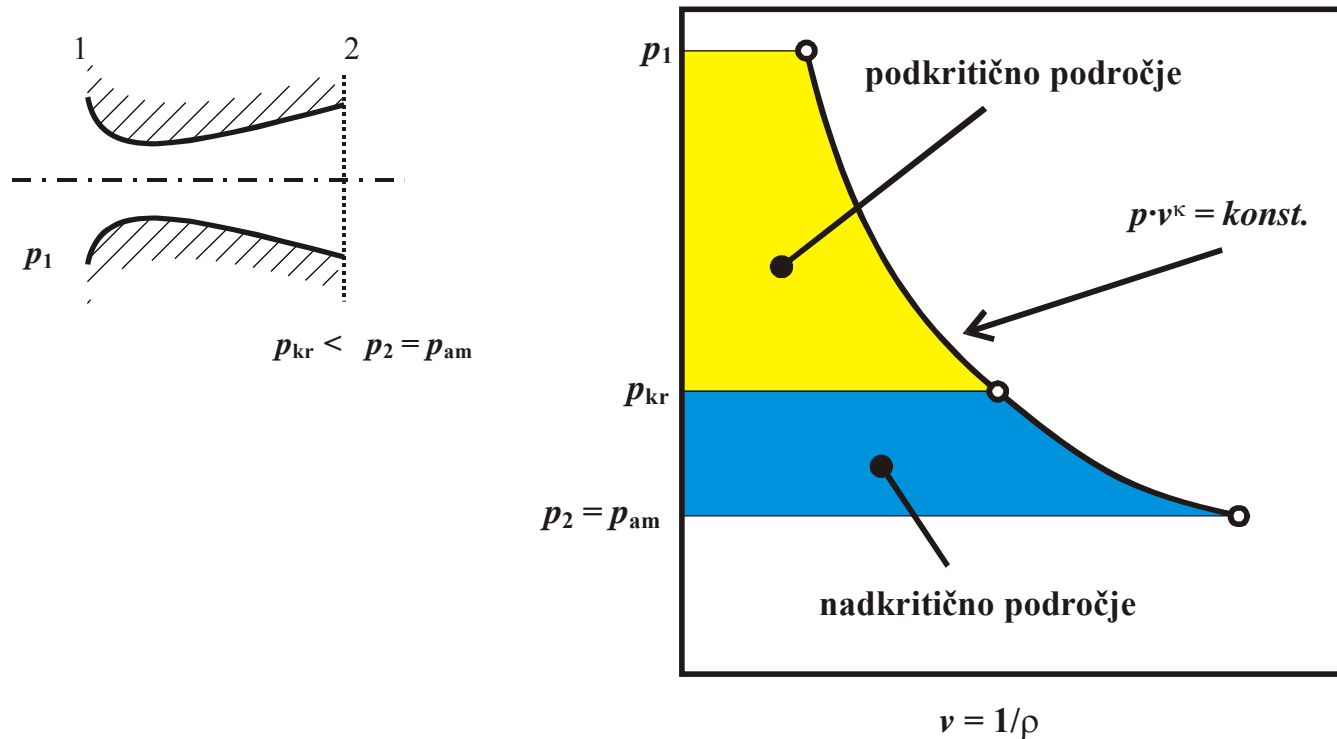
Zvočna hitrost je veličina stanja, saj je odvisna od lokalnega stanja (T_2) in od plina (κ , R)



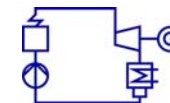
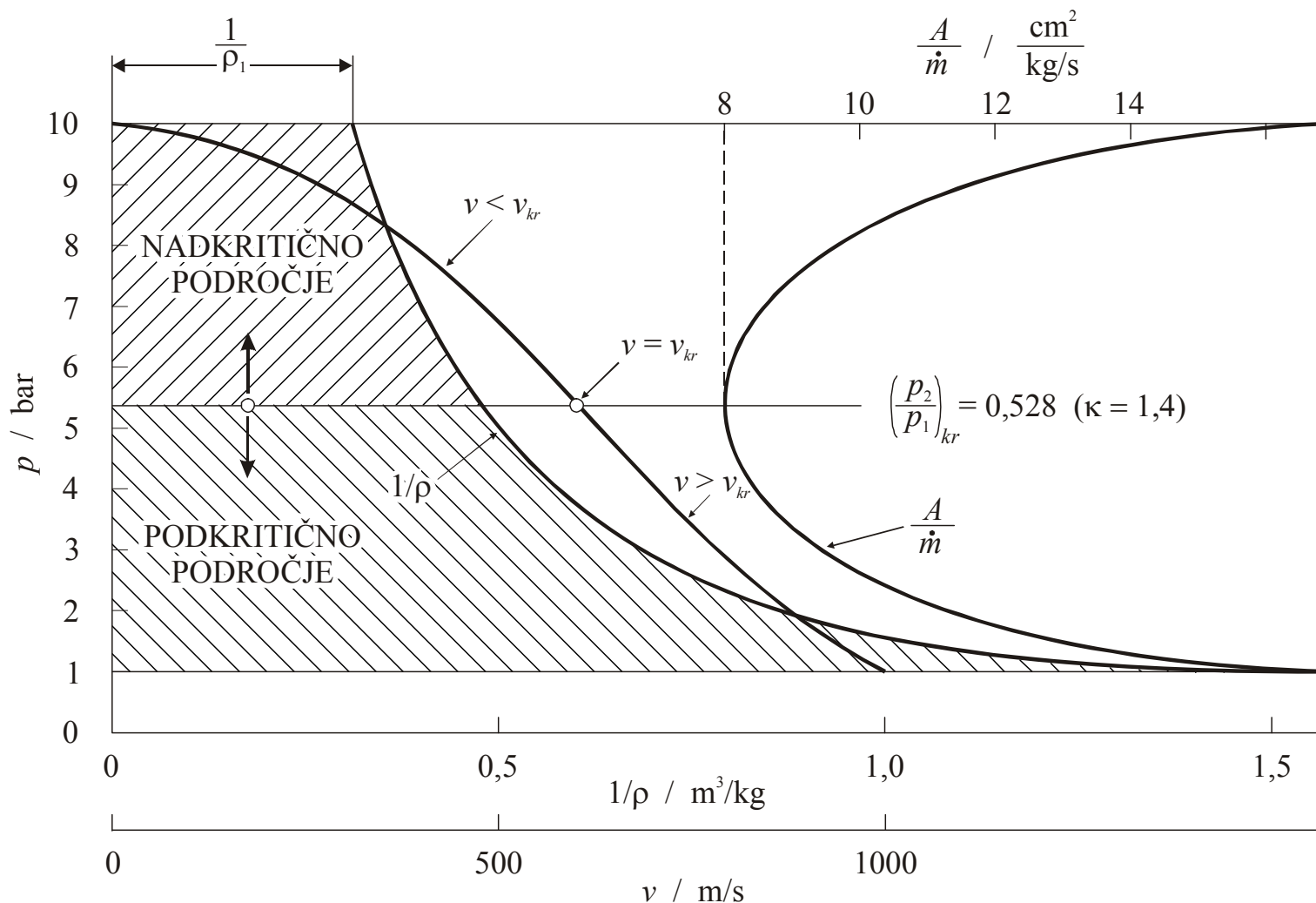


Konvergentno-divergentna šoba:

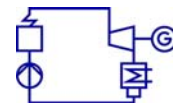
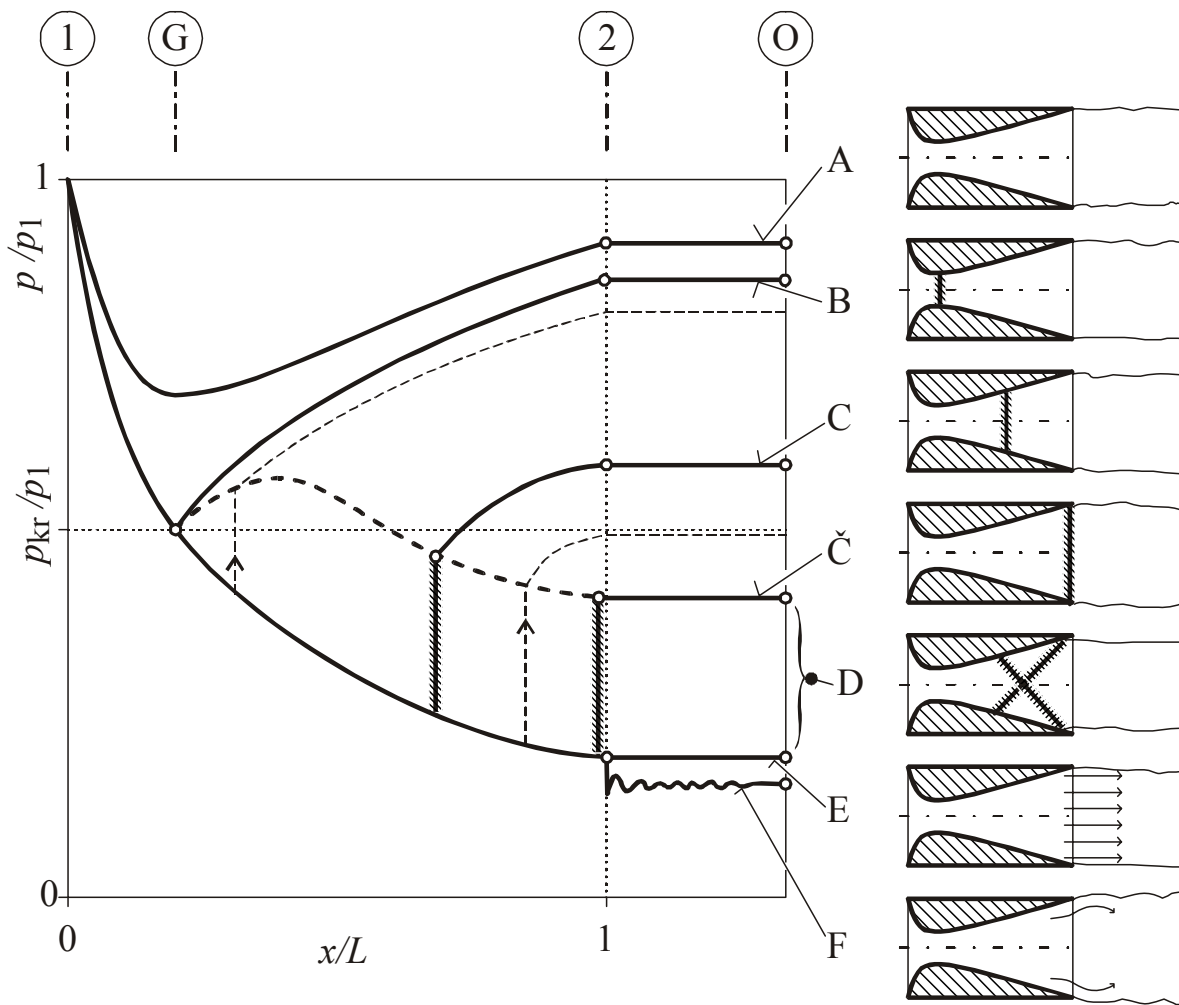
$$\left(\frac{p_2}{p_1}\right) < \left(\frac{p_2}{p_1}\right)_{kr} \Rightarrow \Psi < \Psi_{max} \Rightarrow \frac{dA}{dl} > 0$$



Razmere v nadzvočni šobi, $p_1 = 10$ bar

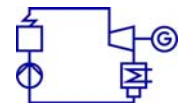
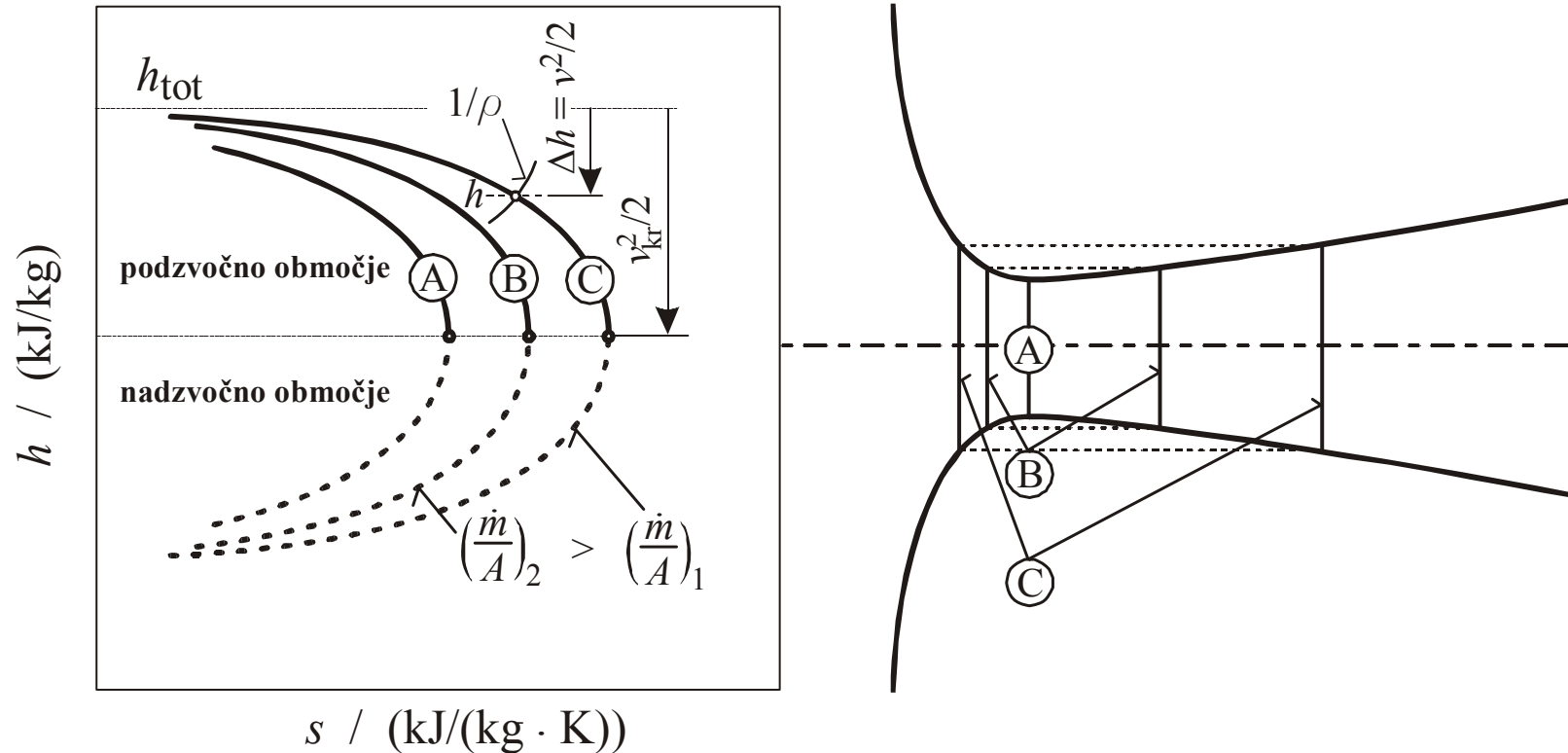


Tlačne razmere v Lavalovi šobi



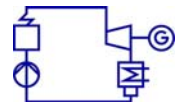
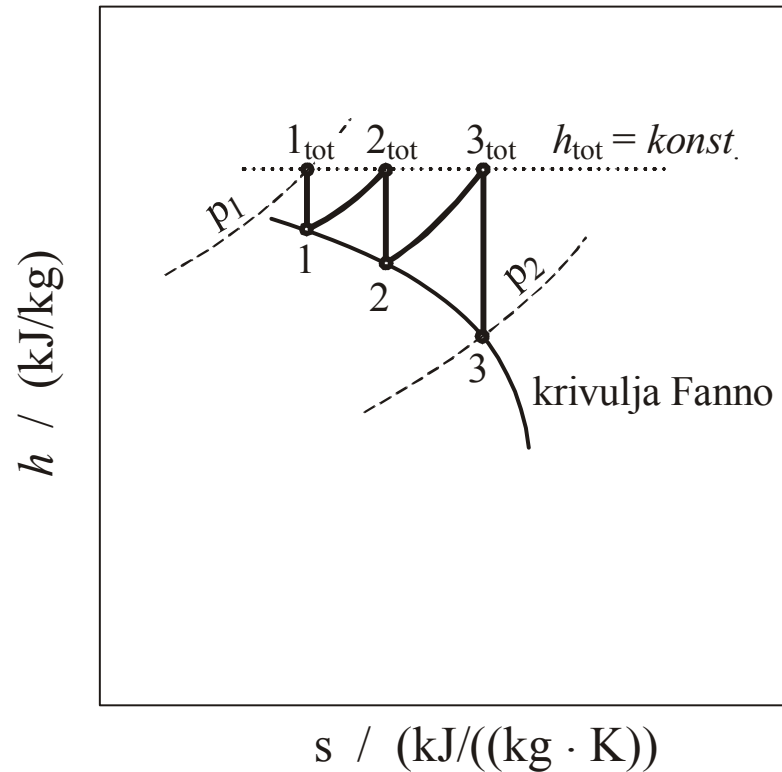
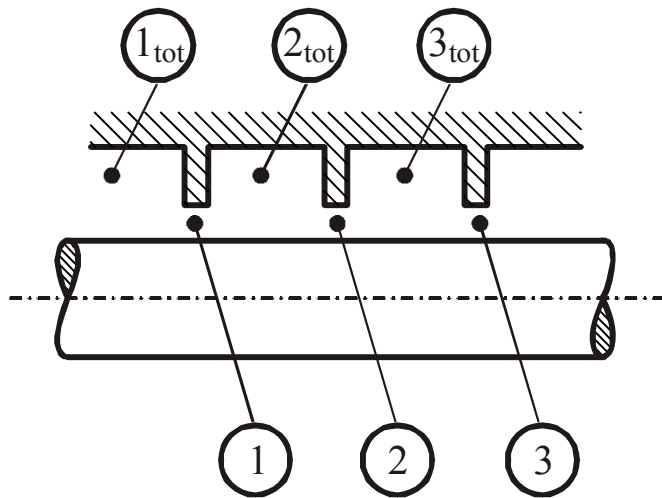
Krivulje Fanno

$$h_{\text{tot}} = h + \frac{v^2}{2} = h + \frac{1}{2 \cdot \rho^2} \cdot \left(\frac{\dot{m}}{A} \right)^2$$



Labirintno tesnenje

$$h_{\text{tot}} = h + \frac{v^2}{2} = h + \frac{1}{2 \cdot \rho^2} \cdot \left(\frac{\dot{m}}{A} \right)^2$$



Prenos toplote

- Prevod toplote : Fourierjev zakon
- Konvekcija in konvektivni prestop toplote
- Sevanje
- Prehod toplote

