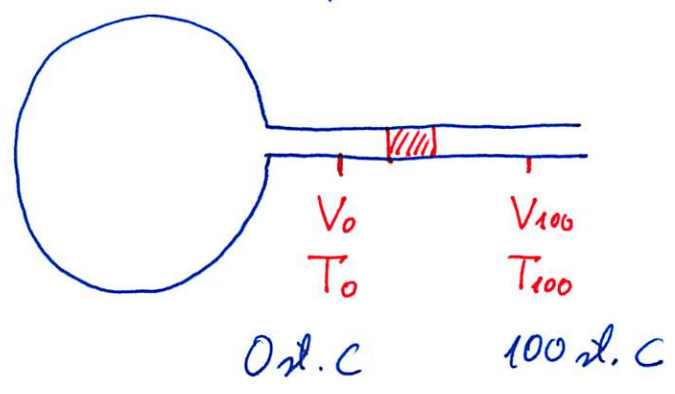
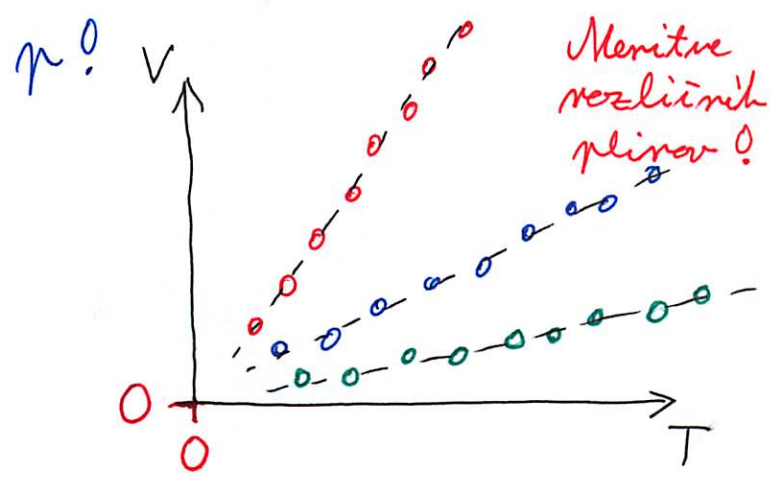


Temperatura

- Makroskopski opis $\sim N_A \sim 10^{23}$ delcev
- Opis neravnovesnih stanj, faznih prehodov
- Termodinamske spremenljivke: p, V, T
- Definicija temperature:

Meritev spremembe volumna v odvisnosti od T pri konstantnem p !



Opozimo, da se vse premice seboja v isti točki, ki ima Volumen (V) $V=0$! Ta točka ima $T=0$ v Kelvinih

$V = k \cdot T$! velja le v Kelvinskih skali

Yemerimo: $\frac{V_{100}}{V_0} = 1,3661 = \frac{T_{100}}{T_0}$ $\rightarrow T_{100} = 1,3661 T_0$

Zahtevamo še $T_{100} - T_0 = 100$
 $1,3661 \cdot T_0 - T_0 = 100$

$T_0 = \frac{100}{0,3661} = 273,15 \text{ K}$!

$T_0 = 273,15 \text{ K} = 0 \text{ st. C} \text{ !}$

$T_K = T_c + 273,15 \text{ K}$ Zmernoik med Kelvinov in Celzijev skalo

$T_F = \frac{9}{5} T_c + 32$ Fahrenheit - ova skala: T_F

Temperaturna raztezaji mami:

Trdnine:

$\Delta l = \alpha l \Delta T$



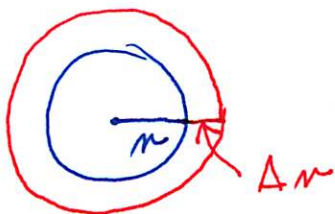
l Δl
raztezek po
segretju za ΔT

α : temperaturni koeficient dolžinskega
razteza

	Δl	medenina	železo	
α	2,4	2	1,2	10^{-5} K^{-1}

Telesine: $\Delta V = \beta V \Delta T$

β : temperaturni koeficient volumskega
razteza $\beta = 3\alpha$



$V + \Delta V = \frac{4\pi}{3} (r + \Delta r)^3 = \frac{4\pi}{3} r^3 + \Delta V$
 $r^3 + 3r^2\Delta r + \dots$

$\Delta V = 4\pi r^2 \Delta r$ $\Delta r = \alpha r \Delta T$
 $\frac{\Delta V}{V} = \frac{4\pi r^2 \Delta r \cdot 3}{4\pi r^3} = 3 \frac{\Delta r}{r} = 3\alpha \Delta T$

Plini, idealni plini

T3

Idealne pline opisuje plinska enota:

$$p \uparrow \quad V \uparrow \quad V = n R T = \frac{m}{M} R T ; \quad R = 8,31 \frac{\text{J}}{\text{mol K}}$$

n : pritisk
 V : volumen
 $n = \frac{m}{M}$: število molar
 M : molarna masa

Opomba: kinetična teorija plinov

Velja tudi:
$$p = \frac{m}{V} \frac{R T}{M} = \rho \frac{R T}{M}$$

Plinska enota predstavlja plin v stanju (p, V, T)

3 dim. prostora

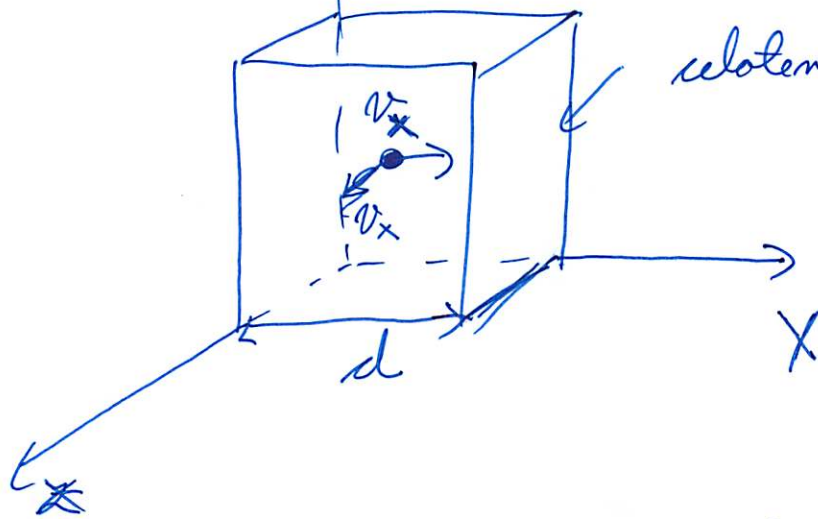
Primer: določi β idealnega plina: $\Delta V = \beta V \Delta T$

$\Rightarrow \beta = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p$: $\left(\frac{\partial V}{\partial T} \right)_p$ je "parcialni" odvod pri konstantnem p ! $V(p, T)$

$$V = \frac{n R}{p} T ; \quad \left(\frac{\partial V}{\partial T} \right)_p = \frac{n R}{p}$$

$$\beta = \frac{1}{V} \frac{n R}{p} = \frac{p}{n R T} \frac{n R}{p} = \frac{1}{T} ; \quad \boxed{\beta = \frac{1}{T}} \text{ idealni plin!}$$

Yajinolina lewisia plinara celoten volumen?



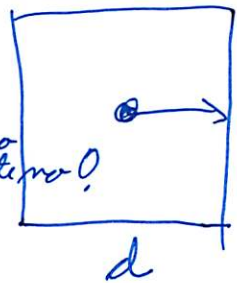
$$V = d^3$$

$$F_{st} \cdot \Delta t = -m v_x - m v_x = -2m v_x$$

$$F_{st} = -\frac{2m v_x}{\Delta t} = -\frac{m v_x^2}{d}$$

prepoteni
vazpalsi 2d sredno
vengura trui ob itosteno!

$$2d = v_x \cdot \Delta t$$



$$F_{st} = \frac{m v_x^2}{d}$$

$$F_{st} = \frac{m}{d} (v_{x1}^2 + v_{x2}^2 + \dots + v_{xN}^2) = \frac{Nm}{d} \overline{v_x^2}$$

$$\overline{v_x^2} = \overline{v_y^2} = \overline{v_z^2} = \frac{1}{3} \overline{v^2}$$

$$F = \frac{Nm}{d} \frac{\overline{v^2}}{3} \quad p = \frac{F}{d^2}$$

$$p = \frac{Nm}{d^3} \frac{\overline{v^2}}{3}$$

$$pV = mRT =$$

$$k_B = 1,38 \cdot 10^{-23} \text{ J/K}$$

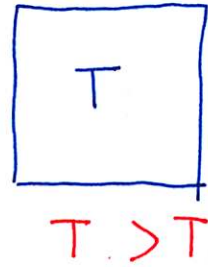
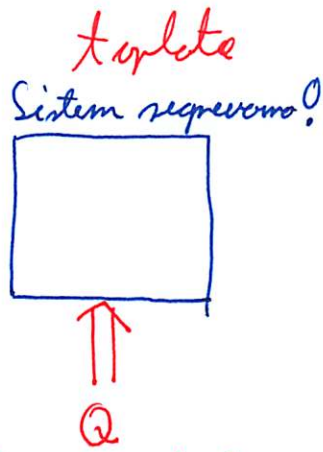
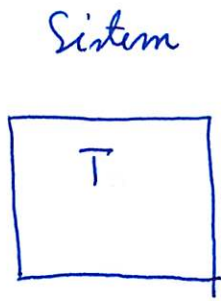
$$N_A = 6,02 \cdot 10^{23} \text{ mol}^{-1}$$

$$pV = N \frac{2}{3} \left(\frac{m \overline{v^2}}{2} \right) = \frac{1}{2} m \overline{v^2} = \frac{3}{2} k_B \cdot T$$

$$= N k_B T = n \cdot \left(N_A k_B \right) T = n R T$$

$$\frac{1}{2} m \overline{v_x^2} = \frac{1}{2} k_B T = \frac{1}{2} m \overline{v_y^2} = \frac{1}{2} m \overline{v_z^2} \quad \text{Eberantirivishi israh!}$$

Definicija toplote; specifitna



dovajamo toplota

previsa se temperaturna sistema

Sistem segrevamo tako, da ga pretvarimo v stih r topljivim



$$Q = m \cdot c \cdot (T_k - T_z) =$$

$$Q = m \cdot c \cdot \Delta T$$

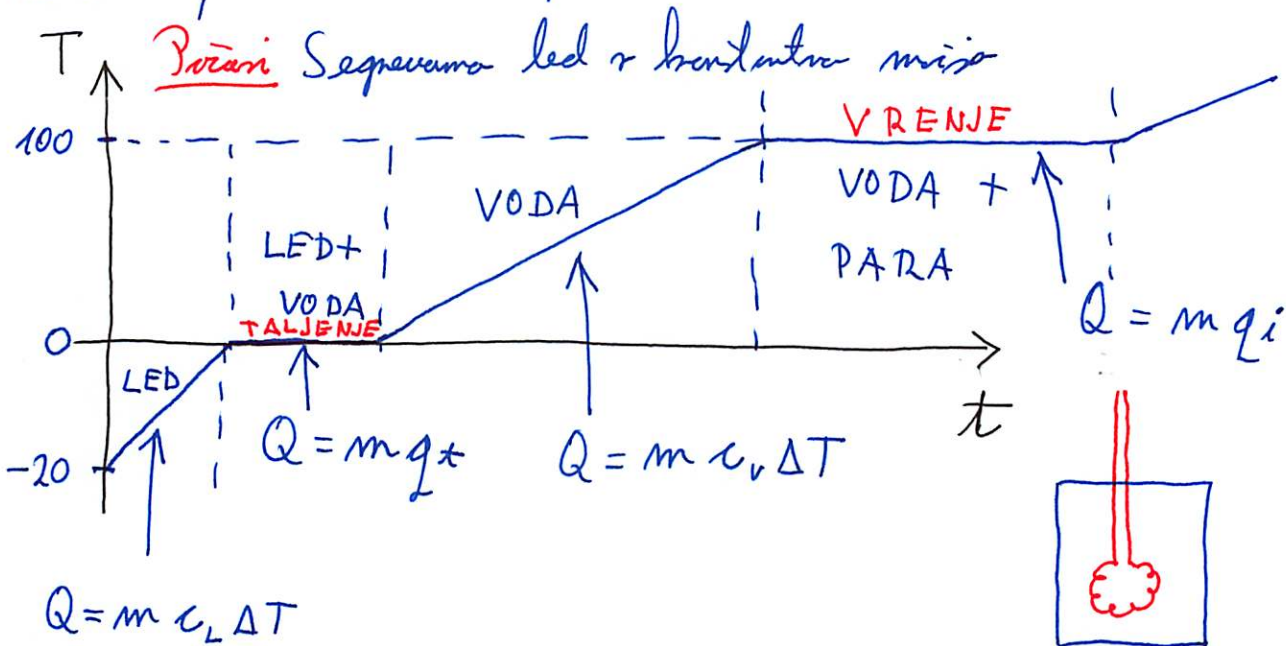
Enote: Q [J] toplota merimo v Joulih;

c : Specifitna toplota [J/kgK]

	c [$\frac{J}{kgK}$]
Železo	128
Alu	236
Al	900
Granit	790
Steklo	840
Led	2100
Voda	4200

Forme spremembe

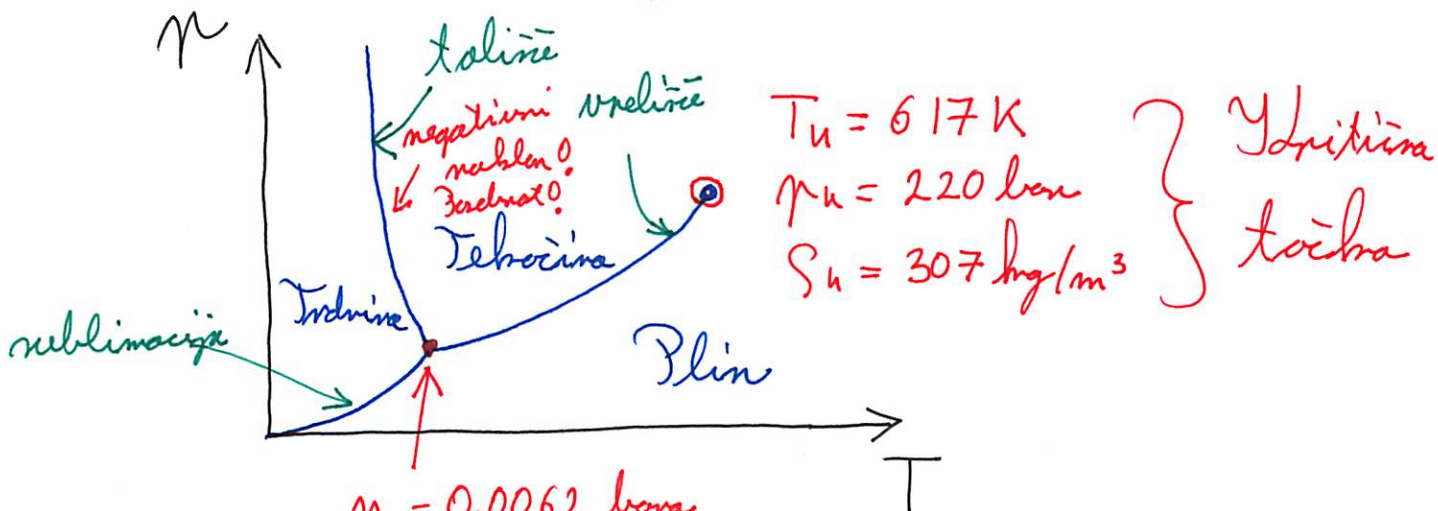
led - voda ; voda - para



$c_L = 2100 \frac{J}{kg \cdot K}$; $c_v = 4200 \frac{J}{kg \cdot K}$

$q_t = 0,336 \frac{MJ}{kg}$; $q_i = 2,26 \frac{MJ}{kg}$
 specifična talilna toplota ; specifična izparilna toplota

Formni diagram vode:

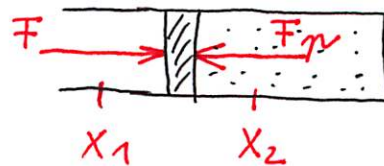


Trojna točka:
 $p_t = 0,0062 \text{ bara}$
 $T_t = 273,16 K$

Delo plina

T6

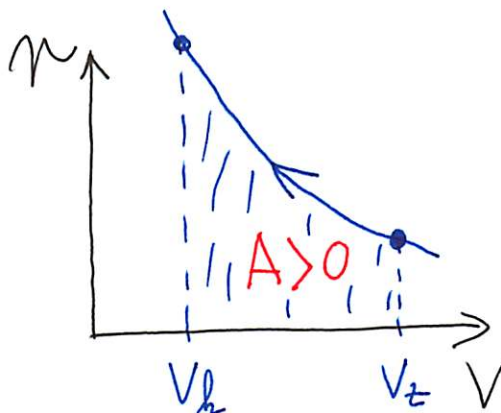
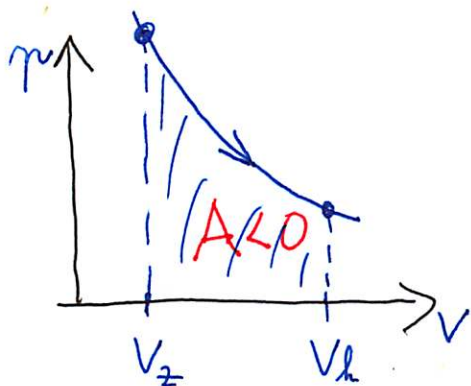
Delo nile:
$$A = \int_{x_1}^{x_2} F dx$$



Yeznozimo ρ

ρ : $F = \rho \cdot S$:
$$A = \int_{x_1}^{x_2} \underbrace{\rho S dx}_{dV} = \int_{V_1}^{V_2} \rho dV$$

Delo plina = - Delo nile \Rightarrow
$$A = - \int_{V_1=V_1}^{V_2=V_2} \rho dV$$



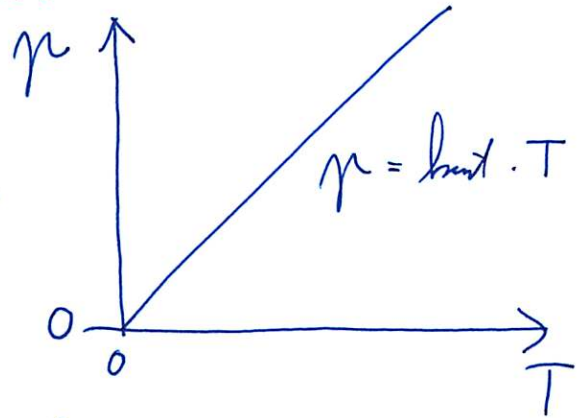
- če se plin širi (rozpenje), je delo negativno oziroma plin delo opravi!
- če se plin krči (stisna), je delo pozitivno oziroma plin delo prejima!

Spromemba na idealnem

Spromemba pri konstantnem V plinca:

a.) Izohorna spromemba
($V = \text{konst.}$)

$$p = \frac{m}{V} R T$$



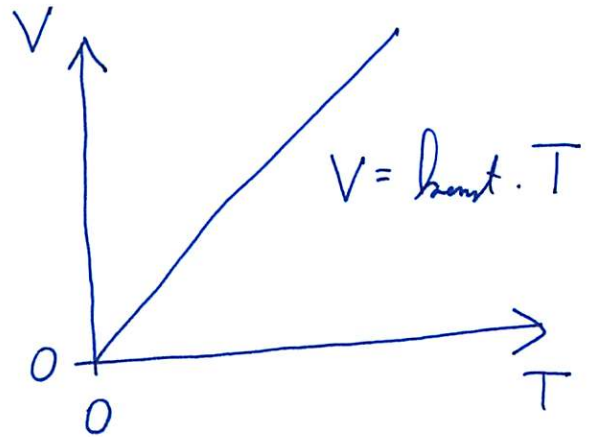
$$\frac{p_1}{T_1} = \frac{p_2}{T_2}$$

$$A = - \int_{V_1}^{V_2} p dV = 0 \text{ ker } V_1 = V_2!$$

$$A + Q = \Delta W_m \Rightarrow Q = \Delta W_m = m c_v \Delta T$$

b.) Spromemba pri konstantnem pritisku ($p = \text{konst.}$)
ali Izobarna spromemba!

$$\frac{V_1}{T_1} = \frac{V_2}{T_2}; \quad V = \frac{m R}{p} \cdot T$$



$$A = - \int_{V_1}^{V_2} p dV = -p \int_{V_1}^{V_2} dV \Rightarrow$$

$$A = -p (V_2 - V_1) \quad \text{Definiramo: } Q = m c_p \Delta T = m c_p (T_2 - T_1)$$

$$A + Q = \Delta W_m$$

$$-p (V_2 - V_1) + m c_p (T_2 - T_1) = m c_v (T_2 - T_1) \quad | : m \cdot (T_2 - T_1)$$

$$c_p = c_v + \frac{p (V_2 - V_1)}{m (T_2 - T_1)} = c_v + \frac{p \Delta V}{m \Delta T} = c_v + \frac{R}{M}$$

$$c_p = c_v + \frac{R}{M}$$

$$p \Delta V = \frac{m}{M} R \Delta T$$

Velja tudi: $A = -p(T_2 - T_1)$

$Q = m c_p (T_2 - T_1)$

$\Delta W_m = m c_v (T_2 - T_1)$

$c_p = c_v + \frac{R}{M}$

Diferenciramo:

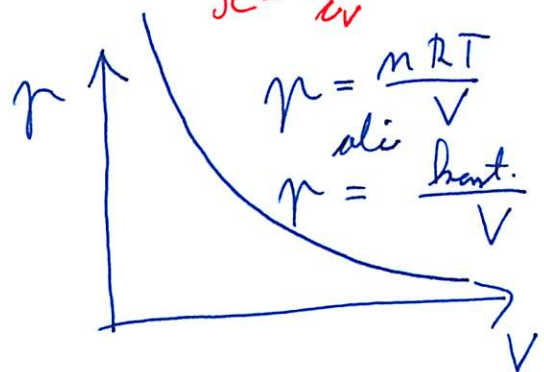
$\alpha = \frac{c_p}{c_v}$

$\alpha = \frac{c_p}{c_v}$

(T3)

c. Sprememba pri konstantni T ali Izoterma sprememba

$p_1 V_1 = p_2 V_2$; $p = \frac{nRT}{V}$



$\Delta W_m = m c_v \Delta T = 0!$

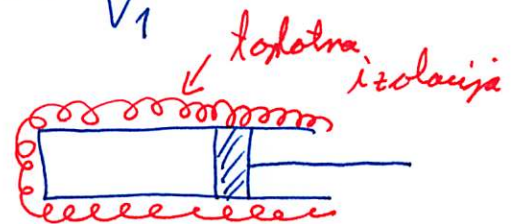
$A + Q = 0 \Rightarrow Q = -A$

$A = - \int_{V_1}^{V_2} p dV = - nRT \int_{V_1}^{V_2} \frac{dV}{V} = - nRT \ln \frac{V_2}{V_1}$
 $p_1 V_1 = p_2 V_2$

$A = - p_1 V_1 \ln \frac{V_2}{V_1}$; $Q = + p_1 V_1 \ln \frac{V_2}{V_1}$

d.) Sprememba na toplota izoliranem sistemu $Q = \text{konstantna}$

izoliranem sistemu $Q = \text{konstantna}$



$A + Q = \Delta W_m$; $dQ = 0$

Velja tudi plinska enačba:

$dA = d(\Delta W_m)$

$-p dV = m c_v dT$

$pV = nRT$

$-\frac{dV}{V} = \frac{m c_v}{nR} \frac{dT}{T} = \frac{M c_v}{R} \frac{dT}{T}$

$p = \frac{nRT}{V} = \frac{mRT}{MV}$

$-\int_{V_1}^{V_2} \frac{dV}{V} = \frac{M c_v}{R} \int_{T_1}^{T_2} \frac{dT}{T} \Rightarrow \ln \frac{V_1}{V_2} = \frac{M c_v}{R} \ln \frac{T_2}{T_1}$

$$\left(\frac{V_1}{V_2}\right)^{\frac{R}{M c_v}} = \frac{T_2}{T_1}$$

$$c_p = c_v + \frac{R}{M} \quad | : c_v$$

$$\gamma = 1 + \frac{R}{M c_v}$$

$$\left(\frac{V_1}{V_2}\right)^{\gamma-1} = \frac{T_2}{T_1} = \frac{V_2 p_2}{V_1 p_1}$$

$$V_1 p_1 = n R T_1$$

$$V_2 p_2 = n R T_2$$

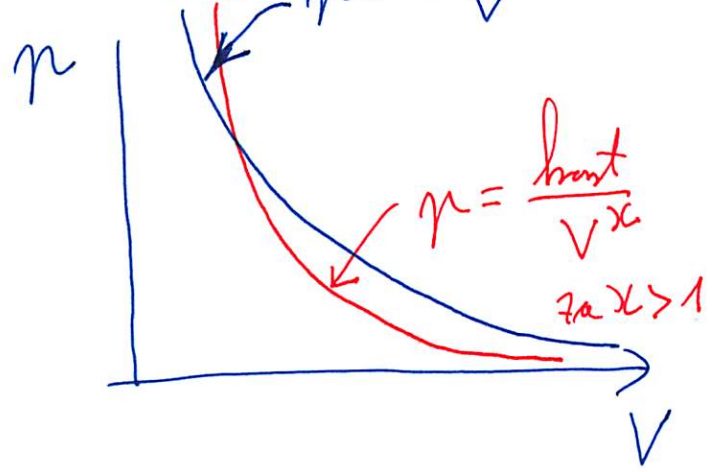
$$\left(\frac{V_1}{V_2}\right)^{\gamma} = \frac{p_2}{p_1}$$

$$\frac{T_1}{T_2} = \frac{V_1 p_1}{V_2 p_2}$$

$$V_1^{\gamma} p_1 = V_2^{\gamma} p_2$$

$$\gamma = \frac{c_p}{c_v} > 1 \quad p = \frac{h_{\text{rost}}}{V}$$

Enočka adiabate!



$$A = \Delta W_m = m c_v (T_2 - T_1) !$$

Entropija

Reverzibilni

Ne reverzibilni procesi

Vzmet

obrat teta ni mogoce

Prozorni odboj zogice

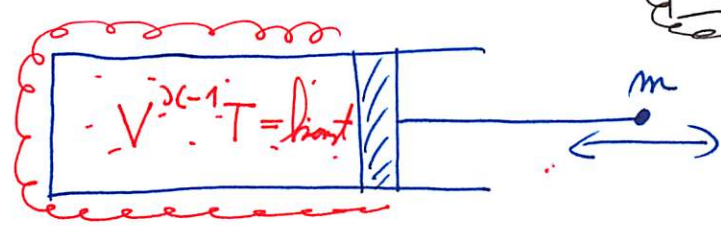
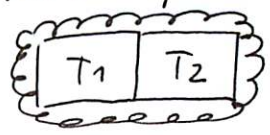
Difuzija kiste v vodi

Adialatno stiskanje

Rozlitje jama

in raztezanje plina

Ylinov paribar



Adialatni proces: $V^{\gamma-1} \cdot T = konst$ / diferencial:

$$V^{\gamma-1} \cdot T : \left((\gamma-1) V^{\gamma-2} T dV + V^{\gamma-1} dT = 0 \right)$$

$$(\gamma-1) \frac{dV}{V} + \frac{dT}{T} = 0$$

za neki spremembe neja:

$$(\gamma-1) \ln \frac{V_k}{V_z} + \ln \frac{T_k}{T_z} = 0$$

Se obrnaji \Leftarrow proces je adialaten \Rightarrow reverzibilen!

Splezni proces

Idealni plin:

$$dW_m = dQ + d$$

$$m c_v dT = dQ - p dV$$



$$\frac{dQ}{T} = m c_v \frac{dT}{T} + \frac{p dV}{T} ; \frac{p}{T} = \frac{m}{M} R \frac{1}{V}$$

$$\frac{dQ}{T} = m c_v \frac{dT}{T} + m \frac{R}{M} \frac{dV}{V}$$

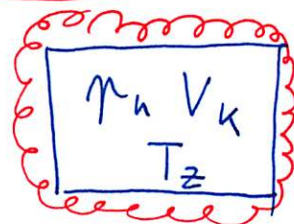
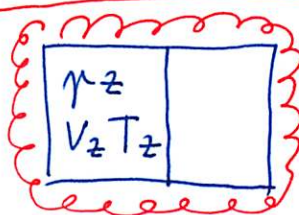
$$\frac{dQ}{T} = m c_v \left(\frac{dT}{T} + \frac{R}{\underbrace{M c_v}_{(x-1)}} \frac{dV}{V} \right) = m c_v \left(\frac{dT}{T} + (x-1) \frac{dV}{V} \right)$$

$$\Delta S \Rightarrow \int \frac{dQ}{T} = m c_v \left(\ln \frac{T_k}{T_z} + (x-1) \ln \frac{V_k}{V_z} \right)$$

↑
veja neevahet!

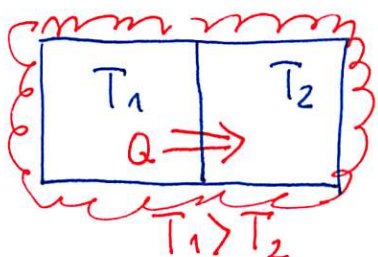
$$\Delta S = m c_v \left(\ln \frac{T_k}{T_z} + (x-1) \ln \frac{V_k}{V_z} \right)$$

Primen: Ilirrav puzhus



$$\Delta S > 0!$$

Toplotno prevozanje



$$\Delta S = -\frac{\Delta Q}{T_1} + \frac{\Delta Q}{T_2} > 0!$$